An Introduction to the Discontinuous Galerkin Method

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Overview

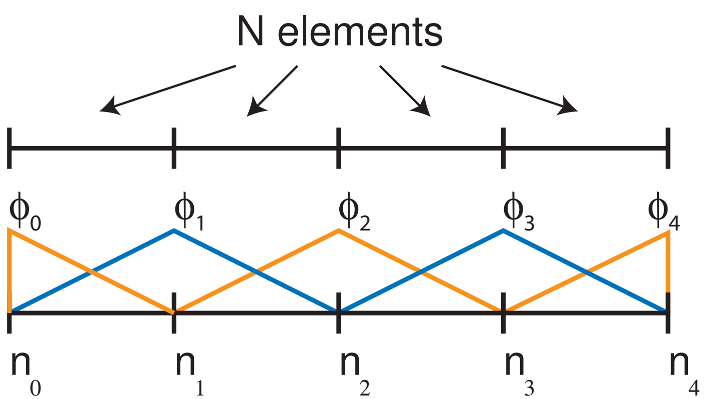
- What is DG? An Example
- Why DG for Computational Fluid Dynamics?
- Project X
- DG vs. Finite Volume
- DG for Elliptic Problems
- p-Multigrid for Higher-order DG Discretizations
- Grid Adaptation
- Conclusions and Ongoing Work

Finite Element Example

- Examine 1-D convection equation with source term:

$$a u_x \quad = \quad cos(x) \quad \text{on} \quad [0, \pi]$$

- Homogenous Dirichlet BCs $\Rightarrow$ Exact solution: $u(x) = \frac{sin(x)}{a}$
- Standard FEM procedure:



- Approximate: $u(x) = \sum_j U_j \phi_j(x)$
- ϕ_j are "hat" basis functions
- $N + 1$ basis functions in 1-D

FEM Example (ctd.)

- Goal: solve for the coefficients U_j (discrete vector $\mathbf{U}$)
- Weak form of equations:

$$\begin{aligned} \int_\Omega a u_x \phi_i dx &= \int_\Omega cos(x)\phi_i dx \\ -\int_\Omega a u \phi_{i,x} dx + \Big[(au)\phi_i\Big]_{\partial\Omega_L}^{\partial\Omega_R} &= \int_\Omega cos(x)\phi_i dx \end{aligned}$$

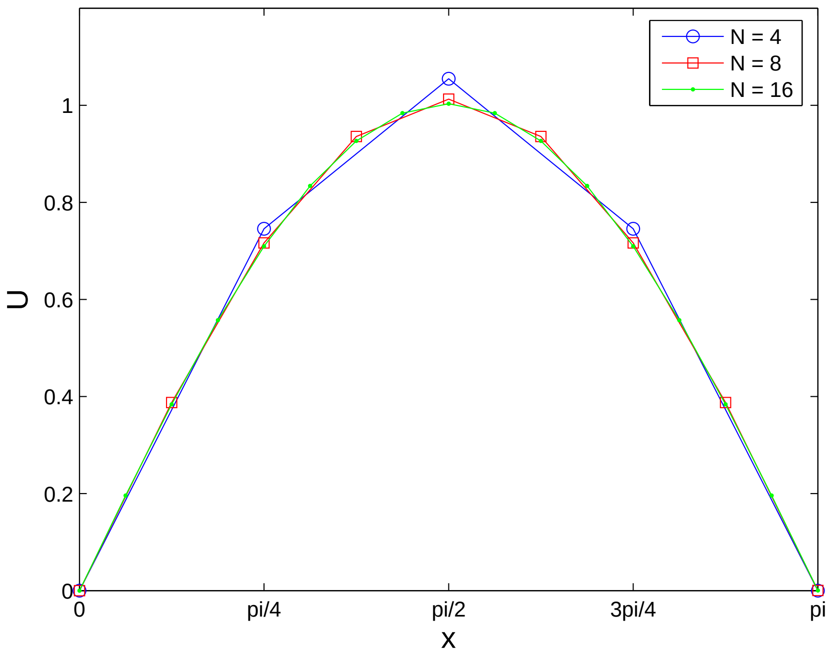
- Substitute $u(x) = \sum_j U_j \phi_j(x)$

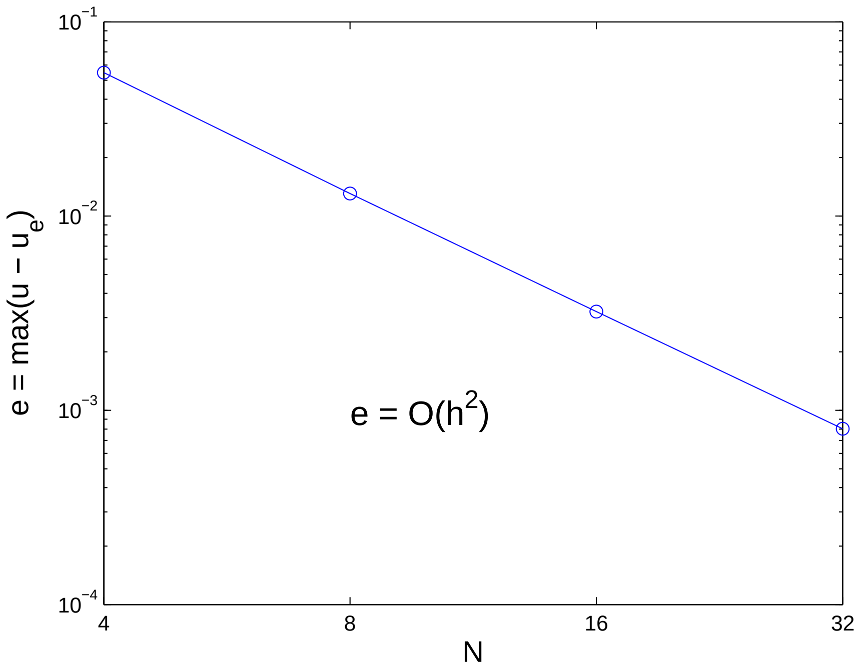
$$-\sum_j U_j \int_\Omega a\phi_j\phi_{i,x} dx + aU_N\phi_i(\pi) - aU_0\phi_i(0) = \int_\Omega cos(x)\phi_i dx$$

Linear System: $\mathbf{A}\mathbf{U} = \mathbf{F}$

Solutions to Example

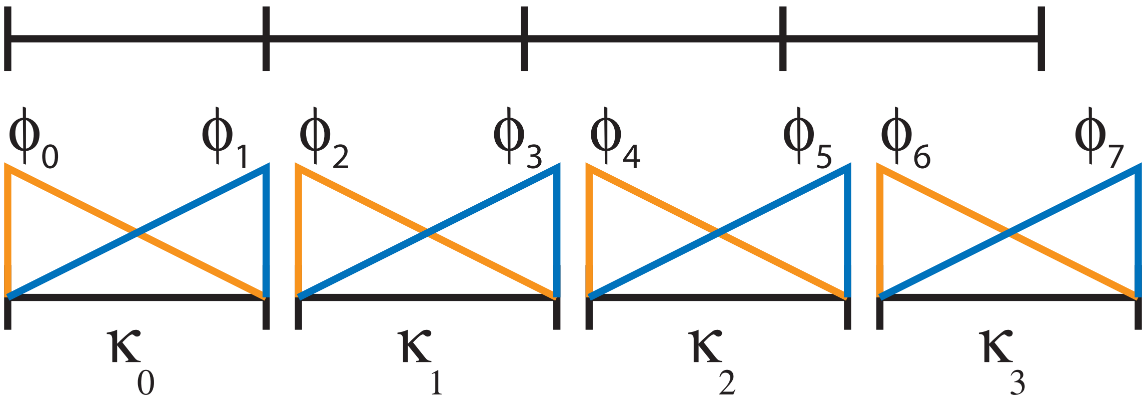
- For a = 1, $u_e = sin(x)$, we obtain:





Where Discontinous Galerkin Differs

- Formulation is the same as standard FEM.
- DG difference is in the choice of basis.
- Specifically, no continuity constraint between elements.



- ϕ_j associated with *elements*.
- $2N$ linear basis functions in 1-D.

DG Weak Form

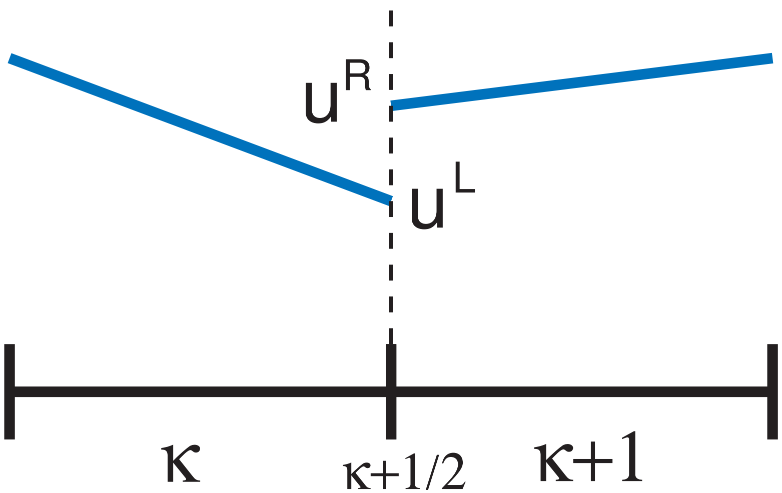
$$
\begin{aligned}
\int_\Omega a u_x \phi_i dx &= \int_\Omega cos(x)\phi_i dx \\
\sum_\kappa \int_\kappa a u_x \phi_i dx &= \sum_\kappa \int_\kappa cos(x)\phi_i dx \\
\sum_\kappa \left\{ -\int_\kappa a u \phi_{i,x} dx + \Big[(au)\phi_i\Big]_{\kappa-1/2}^{\kappa+1/2} \right\} &= \sum_\kappa \int_\kappa cos(x)\phi_i dx \\
-\int_\kappa a u \phi_{i,x} dx + \Big[(au)\phi_i\Big]_{\kappa-1/2}^{\kappa+1/2} &= \int_\kappa cos(x)\phi_i dx
\end{aligned}
$$

What About Element Interfaces?

- Discontinuity creates problem in the weak form:

$$-\int_\kappa au\phi_{i,x}dx + \Big[(au)\phi_i\Big]_{\kappa-1/2}^{\kappa+1/2} = \int_\kappa cos(x)\phi_i dx$$

- (au) is multi-valued at element interfaces.



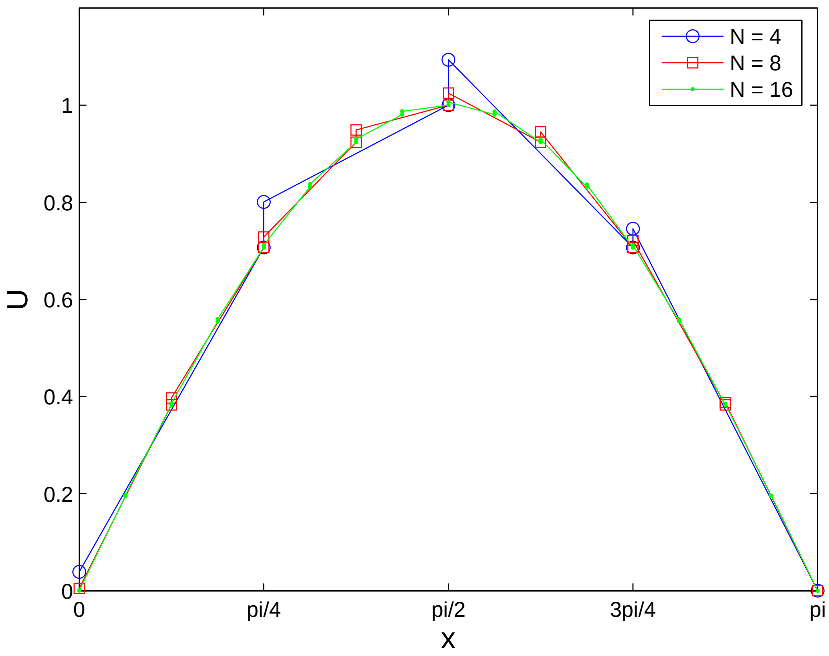
- Fortunately, this problem has been well studied by the Finite Volume community.
- Solution: use numerical flux function

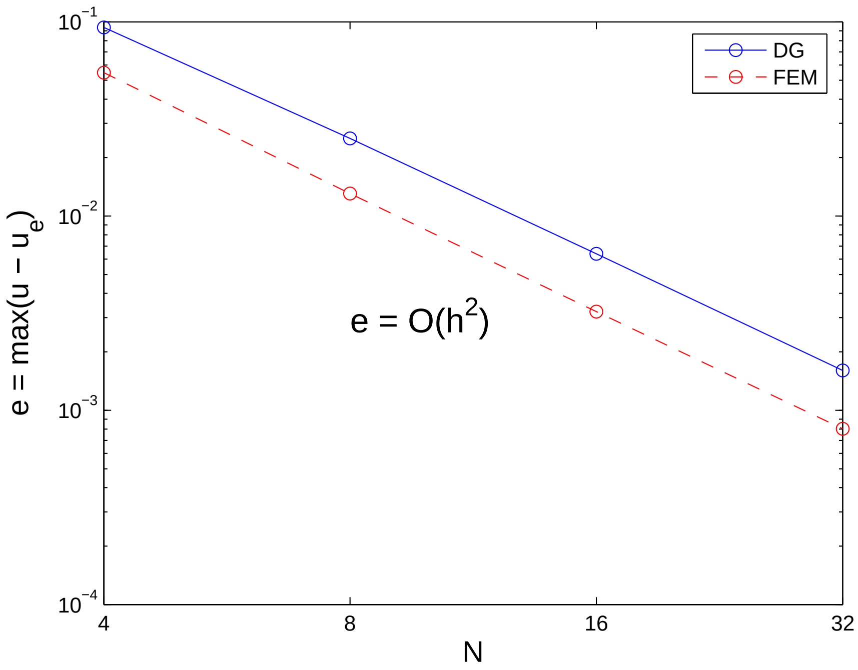
$$(au) \rightarrow \mathcal{H}(u^L, u^R, a).$$

- In this case use pure upwinding.

DG Solution

- For the same 1-D problem, $u_e = sin(x)$, we obtain:



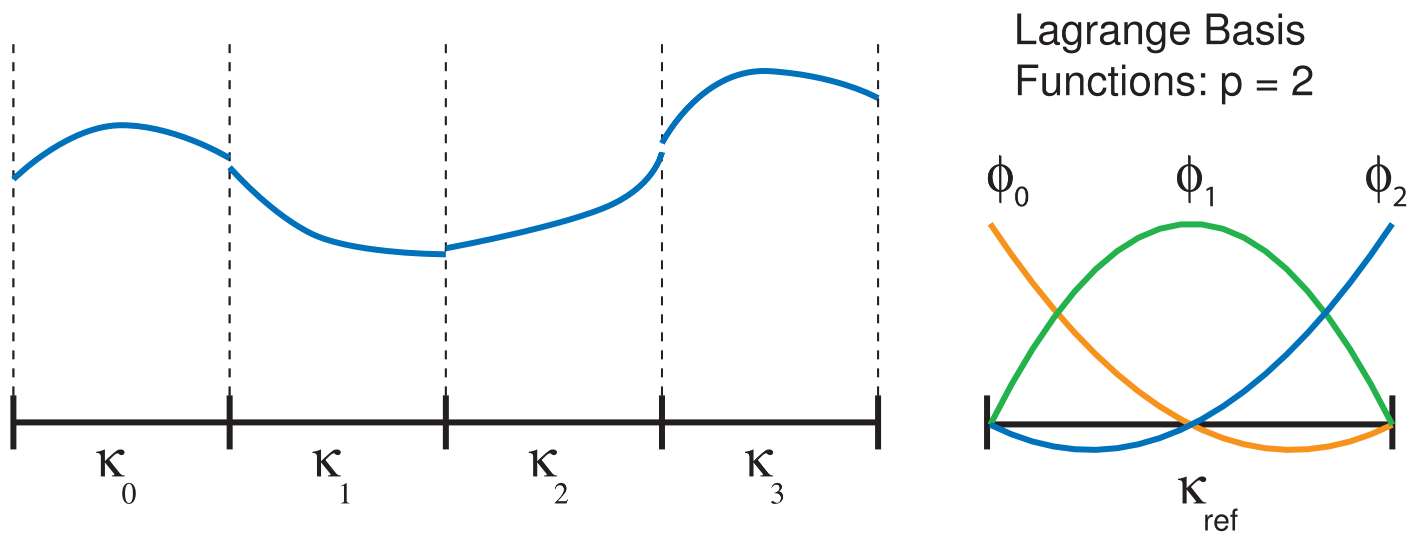


Why DG?

- DG seems to add additional DOFs for no reason.
- Why do we want to use DG over standard FEM?

- Main Benefit:

  Easy to Introduce Higher Order $(p > 1)$ interpolation



(p + 1) Basis Functions per element

Other Benefits of DG

- Basic iterative solution schemes (e.g. block Jacobi) are stable for higher order (i.e. no need for multistaging).
- Discretization lends itself to solution via p-multigrid.
- Easy parallelization.

- In the field of CFD for aerodynamics, these benefits seem to outweigh the cost of extra DOFs.

Project-X

- DG solver package for computational fluid dynamics.
- Started in the Fall of 2002.
- Involved in seven M.S. theses and six ongoing Ph.D. theses.
- Currently:
  - Approximately 100,000 lines of code.
  - Capability ranges from grid generation to visualization.
  - Various side projects: grid adaptation, geometry optimization, turbulence modeling, shock limiting, unsteady studies.
  - End goal is full Reynolds-Averaged Navier-Stokes in 3-D.

Project-X Goal

- Project X Team Goal:
  - To improve the aerothermal design process for complex 3D configurations by significantly reducing the time from geometry to solution at engineering-required accuracy using high-order adaptive methods

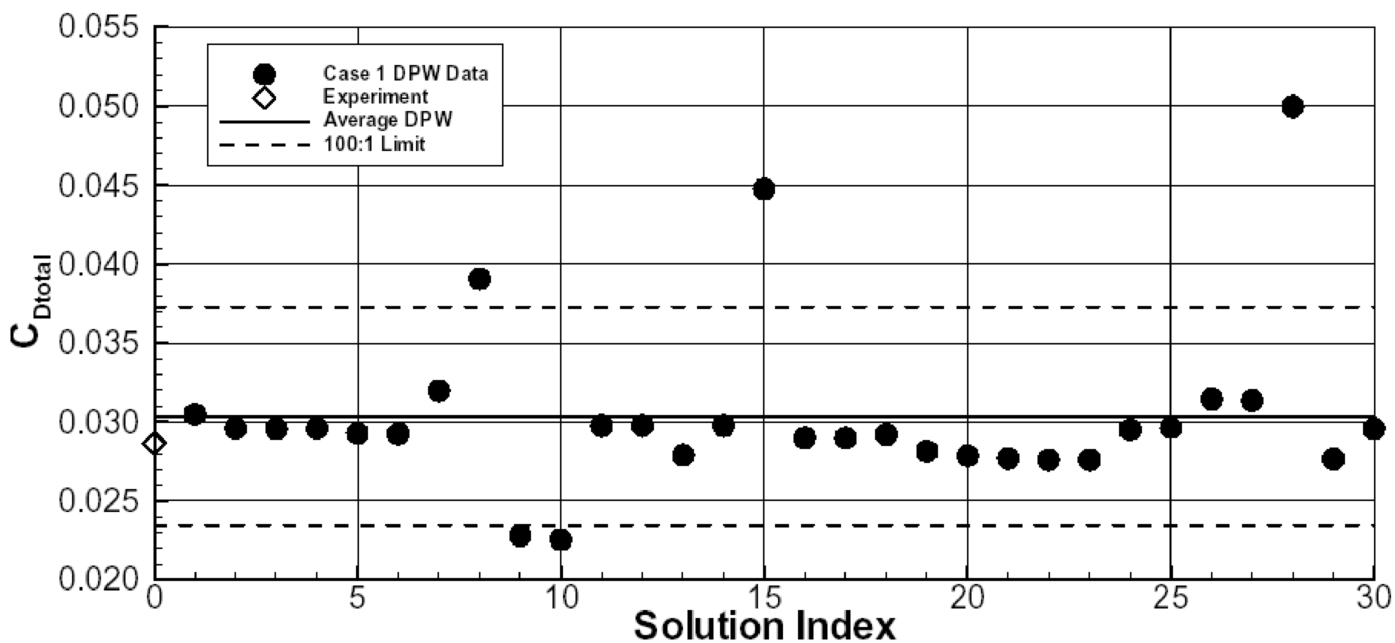
Who are we?

- Todd Oliver
- Chris Fidkowski
- Garrett Barter
- Bob Haimes
- Prof. David Darmofal
- Prof. Jaime Peraire
- Tan Bui
- Shannon Cheng
- James Lu
- Pete Whitney
- Doug Quattrochi

Accuracy of Current CFD Methods

Results of an AIAA Drag Prediction Workshop comparing the performance of industry-standard CFD codes:

AIAA-2002-0841



Motivation for higher order in CFD

- State of CFD in applied aerodynamics
  - Finite-volume with at best second order accuracy
  - Questions exist whether current discretizations are capable of achieving desired accuracy levels in practical time
- Decrease computational time and gridding requirements by increasing solution order

$$\log T = wd\Big(-\frac{1}{p}\log E + \log p\Big) - \log F + const$$

- T = time to solution
- p = discretization order
- E = desired error level ($E << 1$)
- w = solution complexity
- d = dimension of problem
- F = computational speed

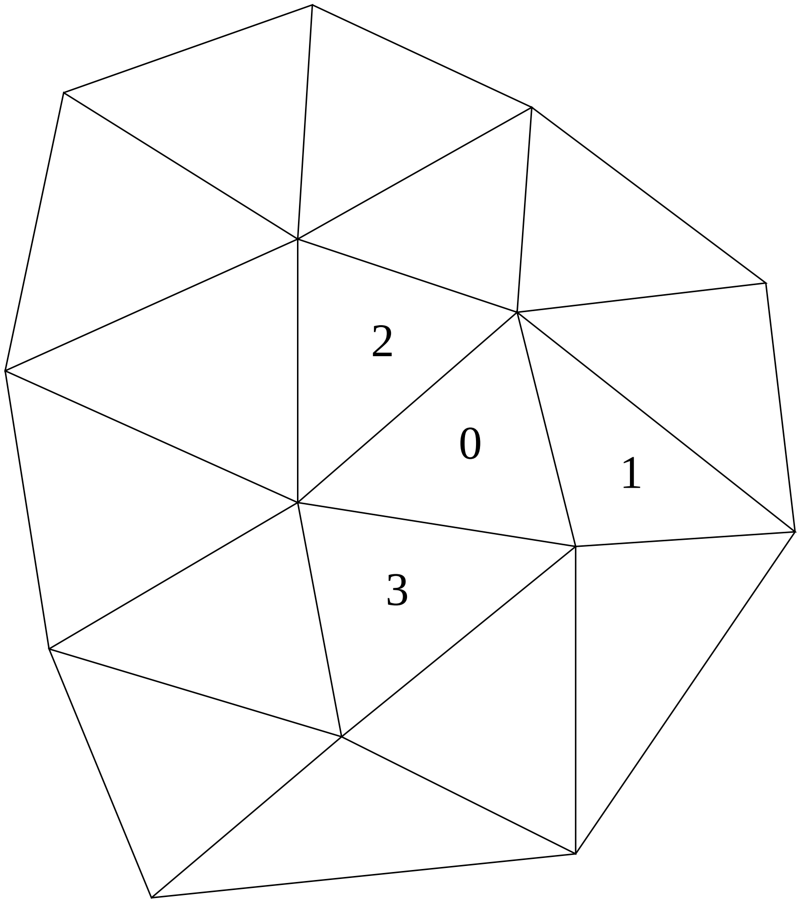
Euler Equations of Gas Dynamics

$$\mathbf{u}_t + \nabla \cdot \mathcal{F}_i(\mathbf{u}) = 0$$

- $\mathbf{u}$ is the state vector and $\mathcal{F}_i$ is the inviscid flux.
- In two dimensions:

$$\mathbf{u} = \begin{bmatrix} \rho \\ \rho u \\ \rho v \\ \rho E \end{bmatrix} \quad \mathcal{F}_i^x = \begin{bmatrix} \rho u \\ \rho u^2 + p \\ \rho u v \\ \rho u H \end{bmatrix}, \quad \mathcal{F}_i^y = \begin{bmatrix} \rho v \\ \rho u v \\ \rho v^2 + p \\ \rho v H \end{bmatrix}.$$

Integral Form

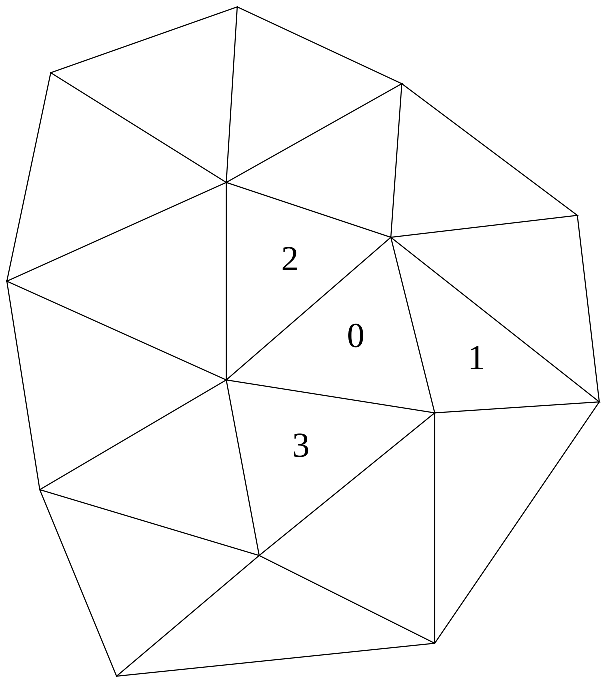


Integrate Euler equations over triangle 0 and use Green's theorem:

$$\frac{d}{dt}\int_{A_0} \mathbf{u}\, d\mathbf{x} + \sum_{k=1}^{3} \int_{0k} \mathcal{F}_i(\mathbf{u}) \cdot \hat{\mathbf{n}}\, ds = 0$$

If we assume $\mathbf{u}$ is constant in each triangle . . .

First-order Accurate Finite Volume



$\mathbf{u}$ constant in each triangle:

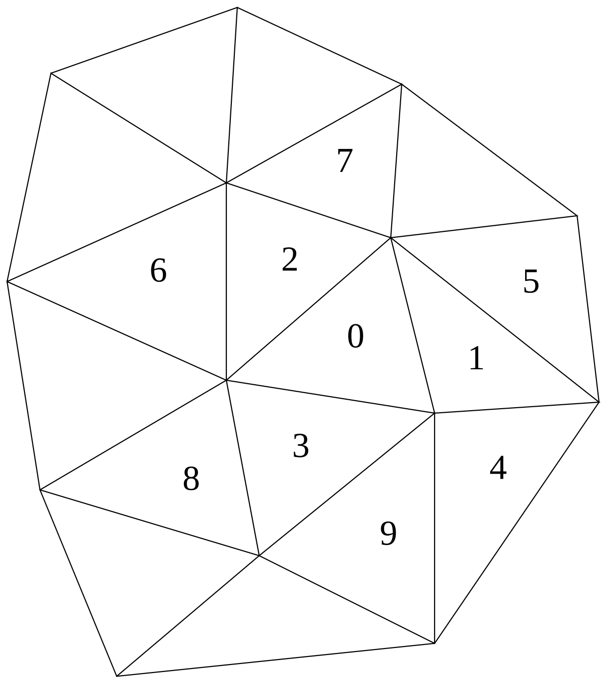
$$\frac{d\mathbf{u}_0}{dt}A_0 + \sum_{k=1}^{3}\int_{0k}\mathcal{H}_i(\mathbf{u}_0, \mathbf{u}_k, \hat{\mathbf{n}}_{0k})\, ds = 0$$

$\mathcal{H}_i(\mathbf{u}_L, \mathbf{u}_R, \hat{\mathbf{n}}_{LR})$ is flux function that determines inviscid flux in $\hat{\mathbf{n}}_{LR}$ direction from left and right states, $\mathbf{u}_L$ and $\mathbf{u}_R$.

Example flux functions: Godunov, Roe, Osher, Van Leer, Lax-Friedrichs, etc.

This discretization has a solution error which is $O(h)$ where h is mesh size.

Second-order Accurate Finite Volume



In each triangle, reconstruct a linear solution, $\tilde{\mathbf{u}}$, using neighboring averages:

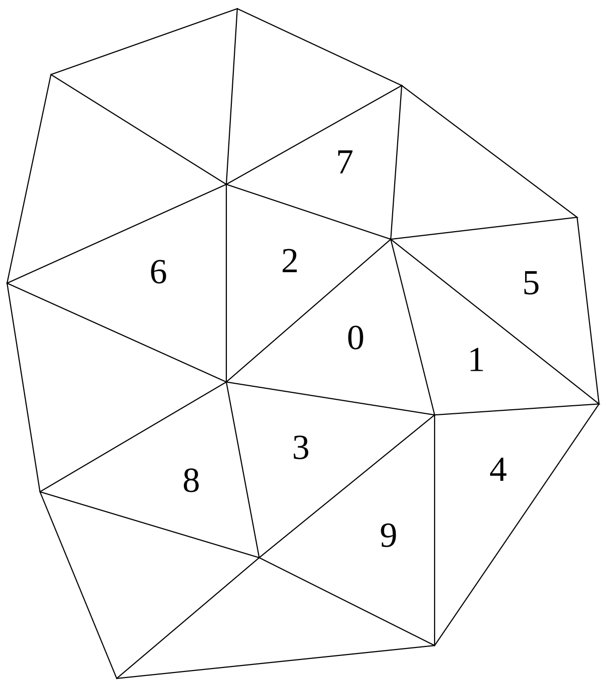
$$\begin{aligned} \tilde{\mathbf{u}}_0 &\equiv \mathbf{u}_0 + (\mathbf{x} - \mathbf{x}_0) \cdot \nabla \mathbf{u}_0, \\ \nabla \mathbf{u}_0 &\equiv \nabla \mathbf{u}_0 \left(\mathbf{u}_0, \mathbf{u}_1, \mathbf{u}_2, \mathbf{u}_3 \right). \end{aligned}$$

Apply conservation law on triangle:

$$\frac{d\mathbf{u}_0}{dt} A_0 + \sum_{k=1}^{3} \int_{0k} \mathcal{H}_i(\tilde{\mathbf{u}}_0, \tilde{\mathbf{u}}_k, \hat{\mathbf{n}}_{0k})\, ds = 0$$

On smooth meshes and flows, solution error is $O(h^2)$.

Pros/Cons of Higher-order Finite Volume



+ Increased accuracy on given mesh without additional degrees of freedom

– Difficulty in achieving higher-order on unstructured meshes and near boundaries

– Stabilizing multi-stage methods necessary for local iterative schemes

– Matrix fill-in results in high-memory requirements

Instability of Local Iterative Methods

Consider steady state problem and define discrete residual for cell j,

$$\mathbf{R}_j(\mathbf{u}) \equiv \sum_{k=1}^{3} \int_{jk} \mathcal{H}_i(\tilde{\mathbf{u}}_j, \tilde{\mathbf{u}}_k, \hat{\mathbf{n}}_{jk})\, ds = 0.$$

A Jacobi iterative method to solve this problem is,

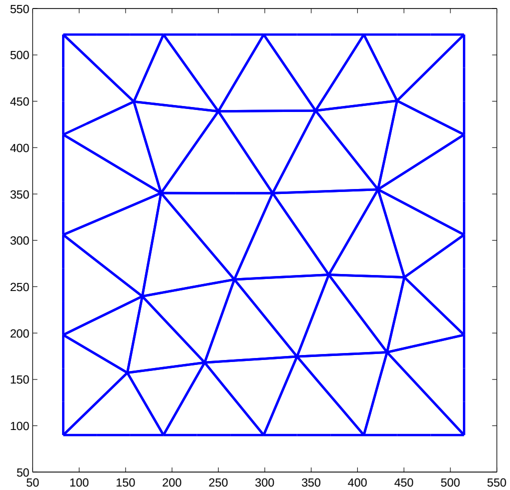
$$\mathbf{u}_j^{n+1} = \mathbf{u}_j^n - \omega \left(\partial \mathbf{R}_j / \partial \mathbf{u}_j\right)^{-1} \mathbf{R}_j(\mathbf{u}).$$

For any finite ω, Jacobi is unstable for higher-order. One solution is a multi-stage method,

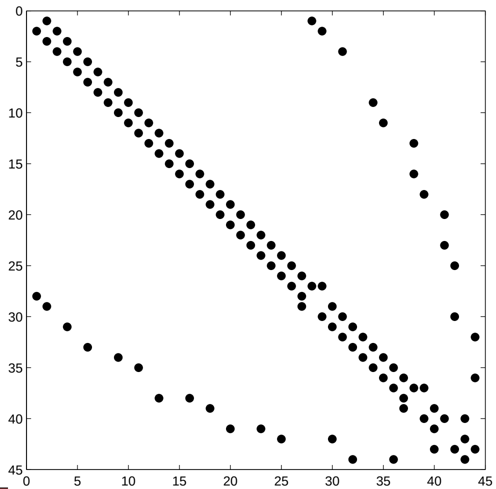
$$\begin{aligned} \hat{\mathbf{u}}_j &= \mathbf{u}_j^n - \hat{\omega} \left(\partial \mathbf{R}_j / \partial \mathbf{u}_j\right)^{-1} \mathbf{R}_j(\mathbf{u}^n) \\ \mathbf{u}_j^{n+1} &= \mathbf{u}_j^n - \omega \left(\partial \mathbf{R}_j / \partial \mathbf{u}_j\right)^{-1} \mathbf{R}_j(\hat{\mathbf{u}}) \end{aligned}$$

$\Leftarrow$ Requires two residual evaluations.

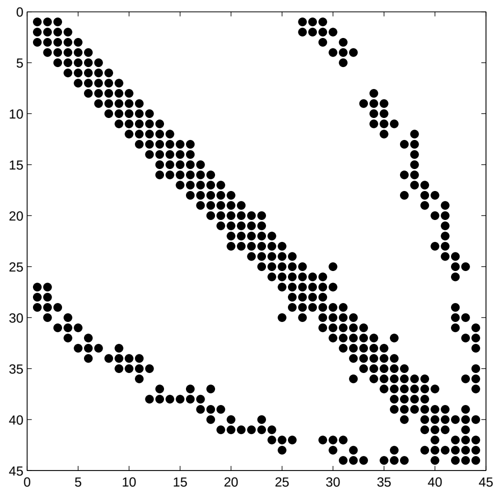
Matrix Fill for Higher-order Finite Volume



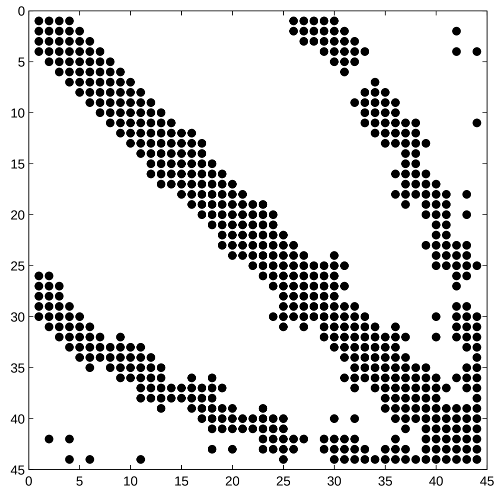
First-order



Second-order



Third-order



DG for the Euler Equations

- Start from strong form of governing equations:

$$\mathbf{u}_t + \nabla \cdot \mathcal{F}_i(\mathbf{u}) = 0.$$

- Look for a solution $\mathbf{u}_h \in \mathcal{V}_h^p$.
- Multiply governing equation by weight function $\mathbf{v}_h \in \mathcal{V}_h^p$ and integrate over element $\kappa \in T_h$:

$$\int_\kappa \mathbf{v}_h^T \left[(\mathbf{u}_h)_t + \nabla \cdot \mathcal{F}_i \right] \, d\mathbf{x} = 0.$$

- Integrate second term by parts (assume interior element):

$$\int_\kappa \mathbf{v}_h^T (\mathbf{u}_h)_t \, d\mathbf{x} - \int_\kappa \nabla \mathbf{v}_h^T \cdot \mathcal{F}_i \, d\mathbf{x} + \int_{\partial\kappa} \mathbf{v}_h^{+T} \mathcal{H}_i(\mathbf{u}_h^+, \mathbf{u}_h^-, \hat{\mathbf{n}}) ds = 0.$$

DG and Finite Volume

- DG weighted residual:

$$\int_{\kappa} \mathbf{v}_h^T (\mathbf{u}_h)_t \, d\mathbf{x} - \int_{\kappa} \nabla \mathbf{v}_h^T \cdot \mathcal{F}_i \, d\mathbf{x} + \int_{\partial\kappa} \mathbf{v}_h^{+T} \mathcal{H}_i(\mathbf{u}_h^+, \mathbf{u}_h^-, \hat{\mathbf{n}}) ds = 0.$$

- For $p = 0$ solution, this reduces to:

$$(\mathbf{u}_\kappa)_t A_\kappa + \int_{\partial\kappa} \mathcal{H}_i(\mathbf{u}_h^+, \mathbf{u}_h^-, \hat{\mathbf{n}}) ds = 0.$$

- Thus, $p = 0$ DG is identical to first-order finite volume.

DG discretization: Global view

- Find $\mathbf{u}_h \in \mathcal{V}_h^p$ such that $\forall \mathbf{v}_h \in \mathcal{V}_h^p$,

$$\sum_{\kappa \in T_h} \left\{ \int_\kappa \mathbf{v}_h^T (\mathbf{u}_h)_t \, d\mathbf{x} - \int_\kappa \nabla \mathbf{v}_h^T \cdot \mathcal{F}_i \, d\mathbf{x} \right\}$$

$$+ \int_{\Gamma_i} \mathbf{v}_h^{+T} \mathcal{H}_i(\mathbf{u}_h^+, \mathbf{u}_h^-, \hat{\mathbf{n}}) \, ds + \int_{\partial\Omega} \mathbf{v}_h^{+T} \mathcal{H}_i^b(\mathbf{u}_h^+, \mathbf{u}_h^b, \hat{\mathbf{n}}) \, ds = 0.$$

- Boundary conditions enforced weakly through $\mathcal{H}_i^b(\mathbf{u}_h^+, \mathbf{u}_h^b, \hat{\mathbf{n}})$ where $\mathbf{u}_h^b$ is determined from desired boundary conditions and outgoing characteristics.
- For smooth problems, the error of this scheme is expected to be $O(h^{p+1})$.

Pros/Cons of Higher-order DG

− Increased accuracy on given mesh requires additional degrees of freedom

\+ Higher-order accuracy not hampered on unstructured meshes nor near boundaries

\+ Local iterative methods are stable

\+ Matrix fill-in maintains block sparsity of $p = 0$

$$\int_\kappa \mathbf{v}_h^T (\mathbf{u}_h)_t \, d\mathbf{x} - \int_\kappa \nabla \mathbf{v}_h^T \cdot \mathcal{F}_i \, d\mathbf{x} + \int_{\partial\kappa} \mathbf{v}_h^{+T} \mathcal{H}_i(\mathbf{u}_h^+, \mathbf{u}_h^-, \hat{\mathbf{n}}) ds = 0.$$

Stability of Local Iterative Methods for DG

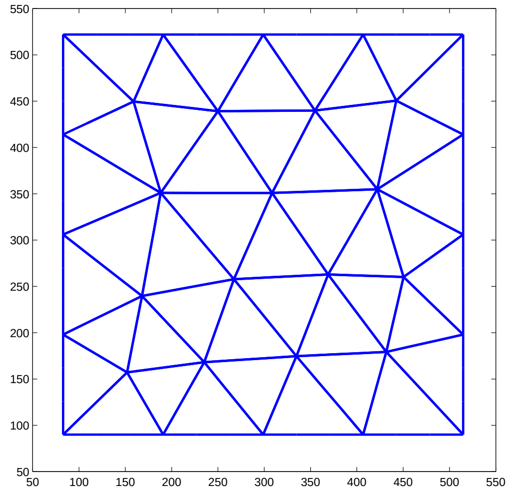
An elemental block Jacobi iterative method to solve this problem is,

$$\mathbf{u}_j^{n+1} = \mathbf{u}_j^n - \omega \left(\partial \mathbf{R}_j / \partial \mathbf{u}_j \right)^{-1} \mathbf{R}_j(\mathbf{u}).$$

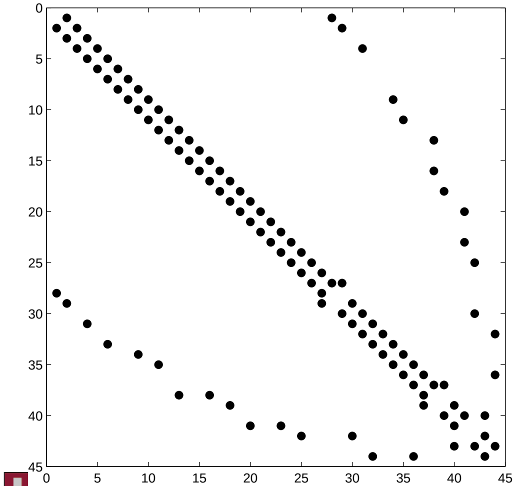
where $\partial \mathbf{R}_j / \partial \mathbf{u}_j$ is the diagonal block for the element j.

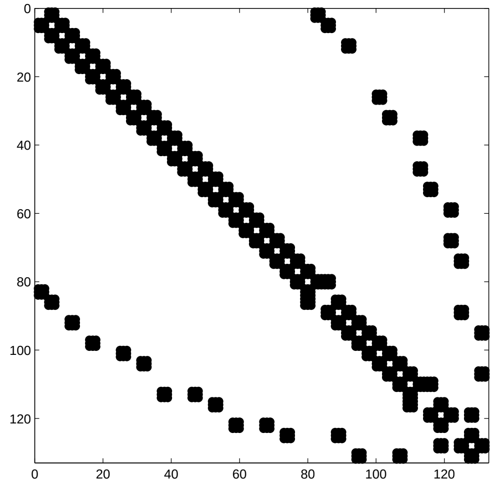
For $0 < \omega < 1$, elemental block Jacobi is stable independent of p.

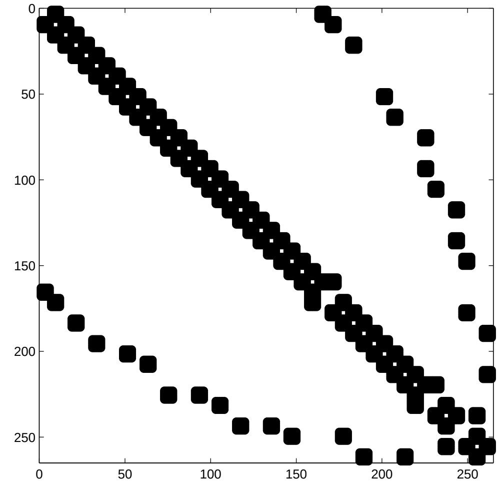
Matrix Fill for Higher-order DG



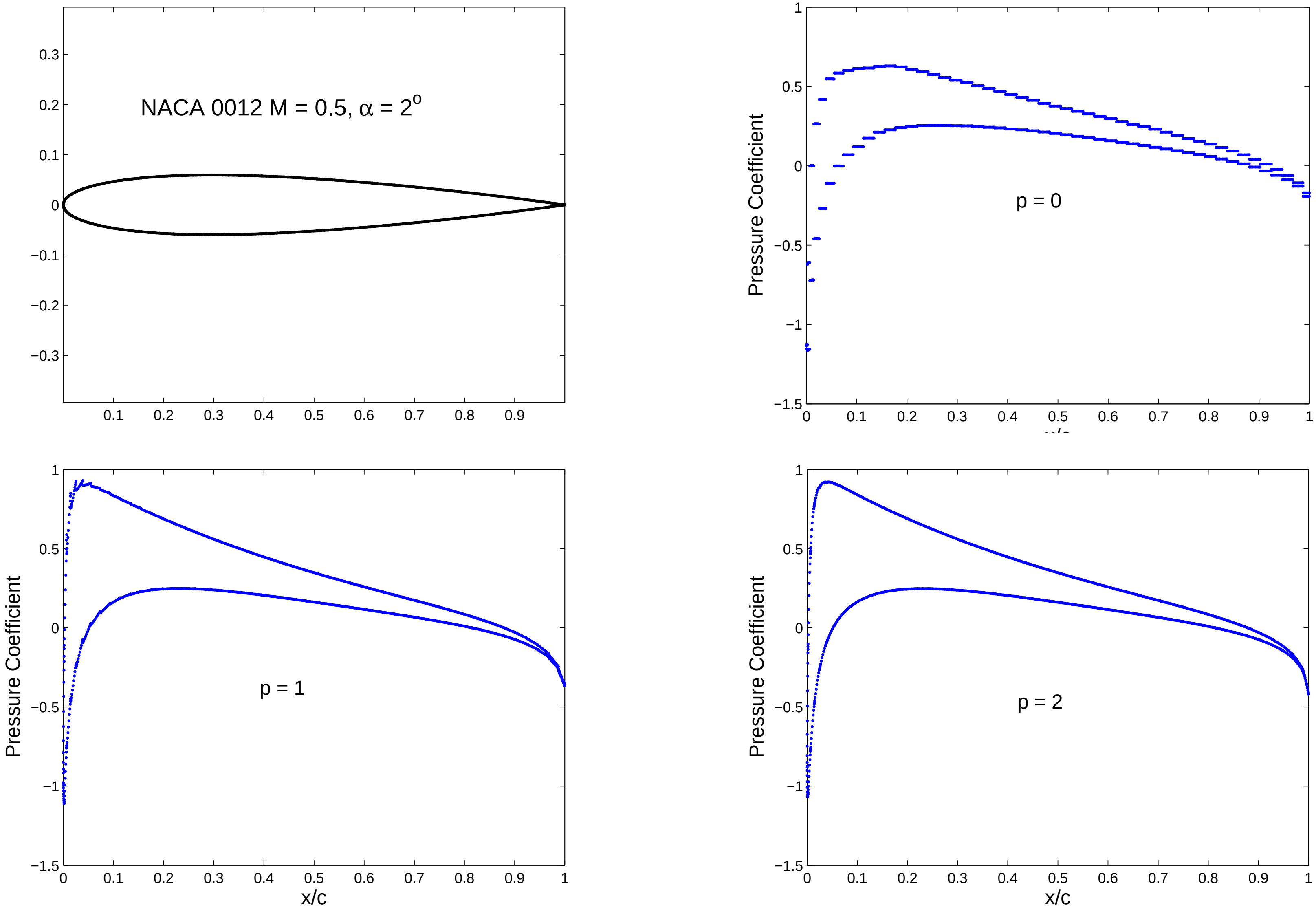
First-order ($p = 0$) | Second-order ($p = 1$) | Third-order ($p = 2$)







Inviscid Flow Example



Navier-Stokes Equations

- Navier-Stokes Equations: $\mathbf{u}_t + \nabla \cdot \mathcal{F}_i(\mathbf{u}) - \nabla \cdot \mathcal{F}_v(\mathbf{u}, \nabla \mathbf{u}) = 0$
- $\mathcal{F}_v = \mathcal{A}_v \nabla \mathbf{u} = (\mathbf{F}_v^x, \mathbf{F}_v^y)$ is the viscous flux vector

$$\mathbf{F}_v^x = \begin{pmatrix} 0 \\ \frac{2}{3}\mu(2\frac{\partial u}{\partial x} - \frac{\partial v}{\partial y}) \\ \mu(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x}) \\ \frac{2}{3}\mu(2\frac{\partial u}{\partial x} - \frac{\partial v}{\partial y})u + \mu(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x})v + \kappa\frac{\partial T}{\partial x} \end{pmatrix},$$

$$\mathbf{F}_v^y = \begin{pmatrix} 0 \\ \mu(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x}) \\ \frac{2}{3}\mu(2\frac{\partial v}{\partial y} - \frac{\partial u}{\partial x}) \\ \frac{2}{3}\mu(2\frac{\partial v}{\partial y} - \frac{\partial u}{\partial x})v + \mu(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x})u + \kappa\frac{\partial T}{\partial y} \end{pmatrix}$$

DG for Elliptic Operators: First Attempt

- Model problem for viscous terms of N-S: 1-D, scalar Poisson's equation

$$-u_{xx} = f \quad \text{on} \quad [-1, 1]$$

- Proceed as for Euler:
  - Triangulate domain into non-overlapping elements $\kappa \in T_h$
  - Define solution and test function space $\mathcal{V}_h^p$
- Discrete formulation: Find $u_h \in \mathcal{V}_h^p$ such that $\forall v_h \in \mathcal{V}_h^p$,

$$\sum_{\kappa \in T_h} \left\{ - \left[v_h \widehat{u_x} \right]_{x_{\kappa-1/2}}^{x_{\kappa+1/2}} + \int_\kappa (v_h)_x (u_h)_x dx \right\} = \sum_{\kappa \in T_h} \left\{ \int_\kappa v_h f dx \right\}$$

- Need to define $\widehat{u_x}$

DG for Elliptic Operators: First Attempt

- No upwinding mechanism $\Rightarrow$ choose central flux

$$\widehat{u_x} = \frac{1}{2}((u_h)_x^L + (u_h)_x^R)$$

- Discrete formulation becomes: Find $u_h \in \mathcal{V}_h^p$ such that $\forall v_h \in \mathcal{V}_h^p$,

$$\sum_{\kappa \in T_h} \Big\{ - \Big[\frac{1}{2} v_h ((u_h)_x^L + (u_h)_x^R)\Big]_{x_{\kappa-1/2}}^{x_{\kappa+1/2}} + \int_\kappa (v_h)_x (u_h)_x dx \Big\} = \sum_{\kappa \in T_h} \Big\{ \int_\kappa v_h f dx \Big\}$$

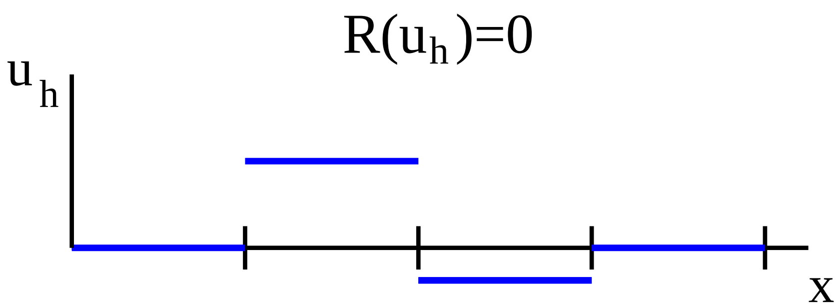
- PROBLEM: Scheme is inconsistent!

Inconsistency

- Examine Laplace's equation with homogeneous Dirichlet BCs

$$\begin{aligned} -u_{xx} &= 0 \quad \text{on} \quad [-1,1] \\ u(-1)=u(1) &= 0 \end{aligned}$$

- Exact solution: $u(x) = 0$



- If $(u_h)_x = 0$ everywhere, discrete equations satisfied exactly regardless of magnitude of u_h

First Order System Approach

- Introduce new variable, $q = u_x$, such that

$$\begin{aligned} -q_x &= f \\ q - u_x &= 0 \end{aligned}$$

- Discrete formulation: Find $u_h \in \mathcal{V}_h^p$ and $q_h \in \mathcal{V}_h^p$ such that $\forall v_h \in \mathcal{V}_h^p$ and $\forall \tau_h \in \mathcal{V}_h^p$,

$$\begin{aligned} \sum_{\kappa \in T_h} \left\{ -\Big[v_h \widehat{q} \Big]_{x_{\kappa-1/2}}^{x_{\kappa+1/2}} + \int_\kappa (v_h)_x q_h dx \right\} - \sum_{\kappa \in T_h} \left\{ \int_\kappa v_h f dx \right\} &= 0 \\ \sum_{\kappa \in T_h} \left\{ \int_\kappa \tau_h q_h dx + \int_\kappa (\tau_h)_x u_h dx - \Big[\tau_h \widehat{u} \Big]_{x_{\kappa-1/2}}^{x_{\kappa+1/2}} \right\} &= 0 \end{aligned}$$

- Need to choose $\widehat{q}$ and $\widehat{u}$

Bassi-Rebay Schemes

- Scheme 1: no upwinding mechanism $\Rightarrow$ choose central fluxes

$$\widehat{u} = \frac{1}{2}(u_h^L + u_h^R); \quad \widehat{q} = \frac{1}{2}(q_h^L + q_h^R)$$

  - Sub-optimal order of accuracy for odd p
  - Stencil no longer compact
- Scheme 2: With $[\![s]\!] = s^L - s^R$ and $\{s\} = 0.5(s^L + s^R)$,

$$\widehat{u} = \{u_h\}; \quad \widehat{q} = \{(u_h)_x\} - \eta_f\{\delta_f\}$$

  - New variable, $\delta_f([\![u]\!])$, is a jump penalty term.
  - Optimal accuracy and compact stencil.

Iterative Solver

- Nonlinear discrete equations can be written

$$\mathbf{R}(\mathbf{u}_h) = 0$$

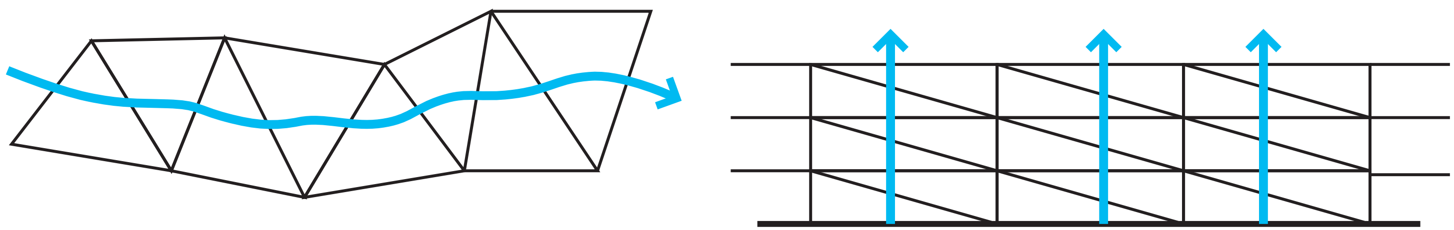
- Use a preconditioned iterative scheme

$$\mathbf{u}_h^{n+1} = \mathbf{u}_h^n - \mathbf{P}^{-1}\mathbf{R}(\mathbf{u}_h^n)$$

- Preconditioner
  - Block-element smoothing
    - $\mathbf{P} = \mathbf{M}_{block} \Rightarrow$ Block diagonal of the Jacobian
  - Line-element smoothing
    - $\mathbf{P} = \mathbf{M}_{line} \Rightarrow$ Block tridiagonal systems from Jacobian

Line Solver

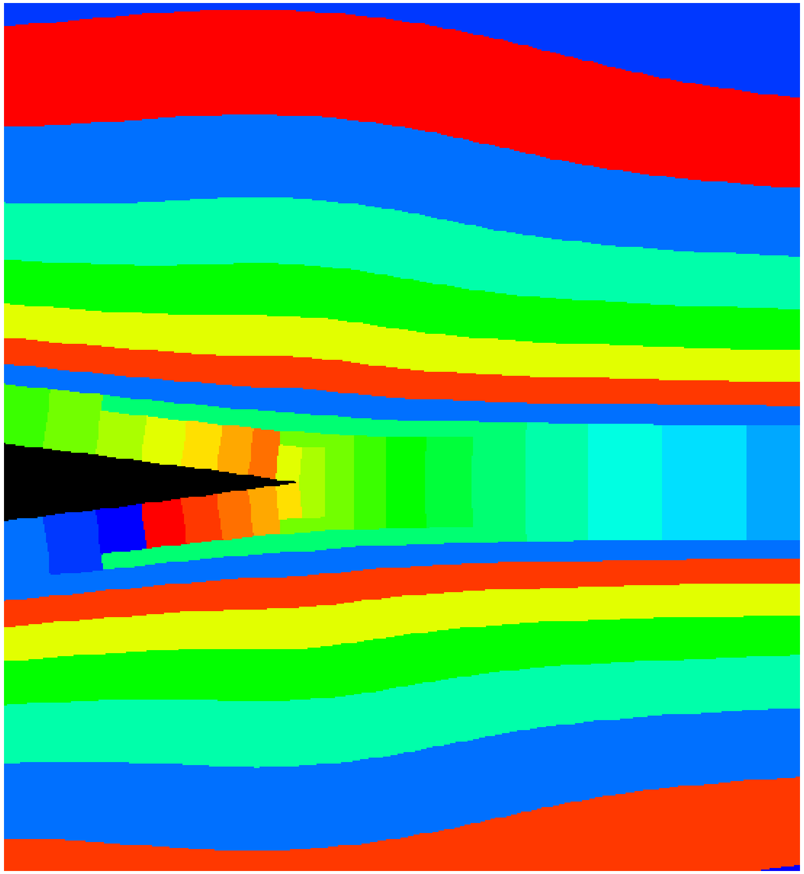
- Motivation: Transport of information in Navier-Stokes equations characterized by convection-diffusion like phenomena
  - Inviscid regions: characteristic directions set by convection
  - Viscous regions: diffusion effects can be stronger

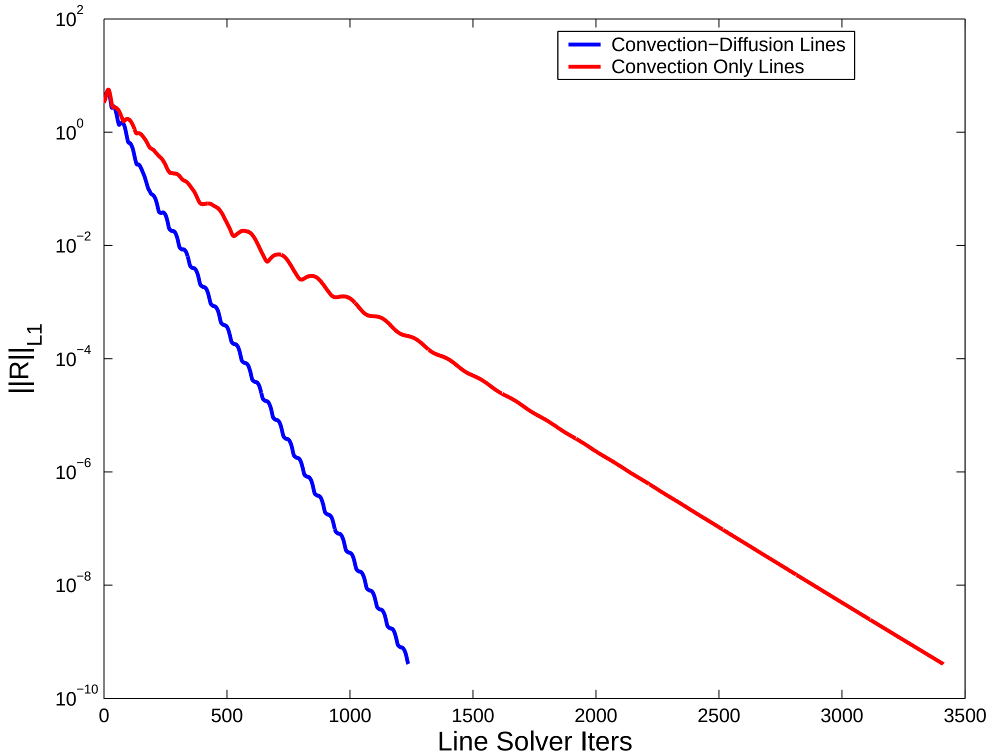


- Procedure:
  - Construct lines of elements based on measure of influence
  - Build and invert $\mathbf{M}_{line}$, which is a set of block tridiagonal systems from the full Jacobian

Example Lines and Performance

Trailing edge of NACA 0012



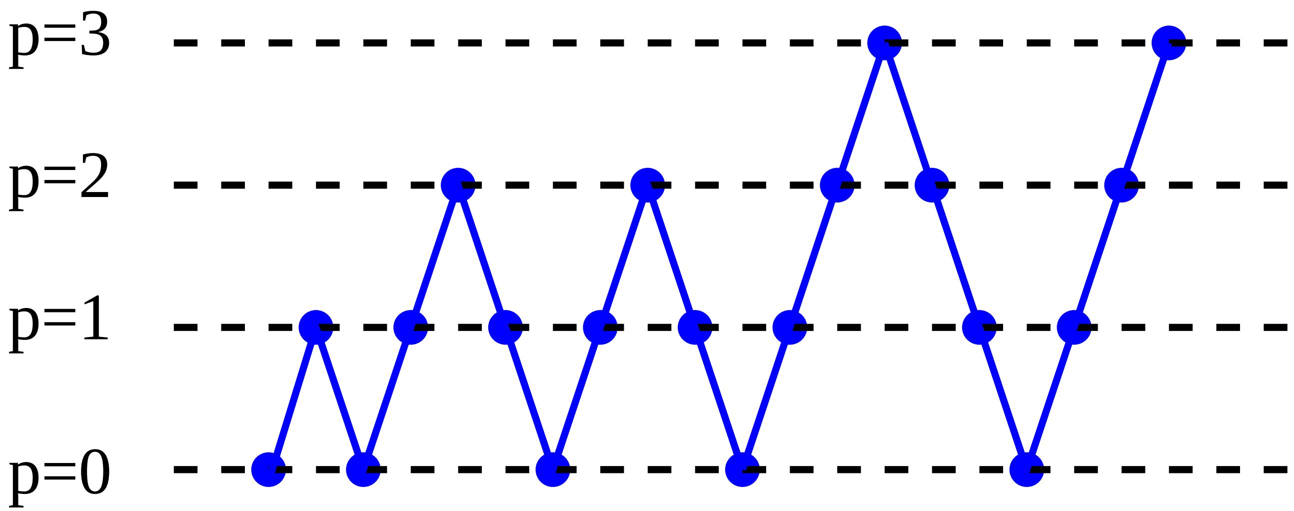


p-Multigrid Solver: Motivation

- Observation: Smoothers are inefficient at eliminating low frequency error modes on fine level
- h-Multigrid
  - Spatially coarse grid used to correct solution on fine grid
  - Grid coarsening is complex on unstructured meshes
- p-Multigrid (Ronquist & Patera, Helenbrook et al., Fidkowski & Darmofal)
  - Low order ($p-1$) approximation used to correct high order (p) solution
  - Natural implementation in DG discretization on unstructured meshes

p-Multigrid Solver: Full Multigrid

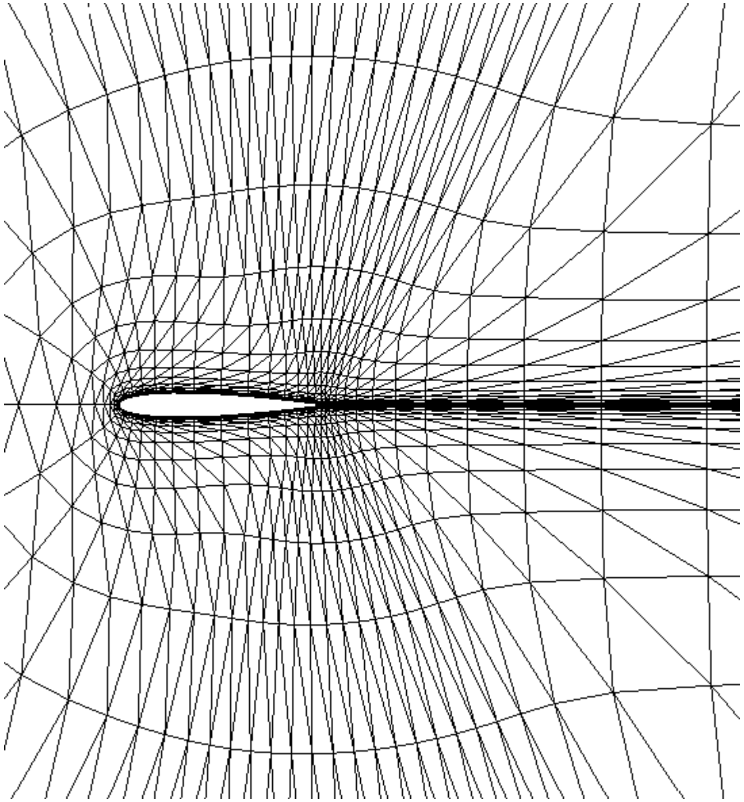
- Iterate on coarsest levels first and use these solutions as initial guesses for fine level solutions.
- Line solver used as smoother
- Full Approximation Scheme (FAS) used to deal with non-linearity



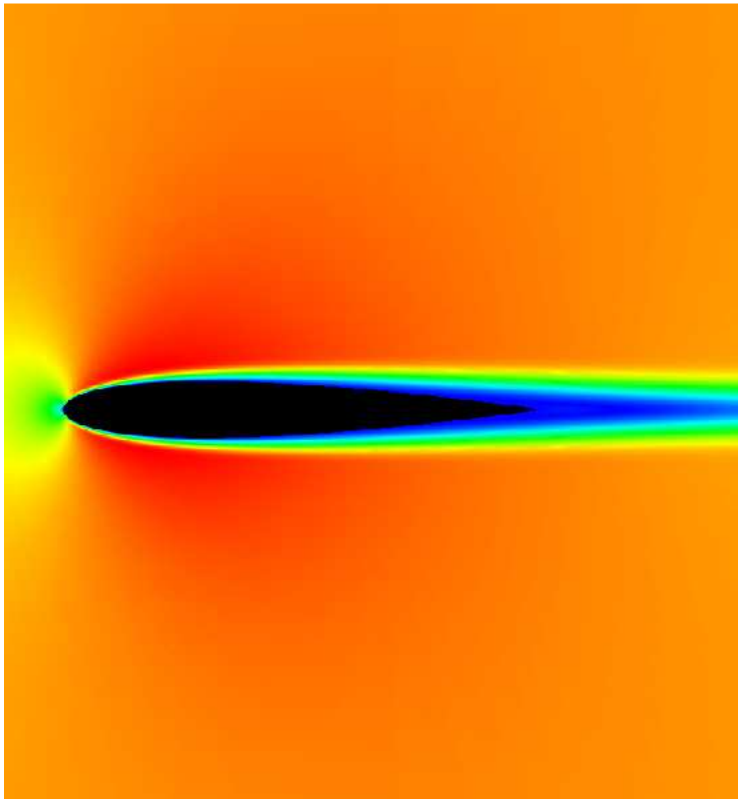
NACA 0012 Test Case

$M = 0.5,\ Re = 5000,\ \alpha = 0$

Grids are from Swanson at NASA Langley

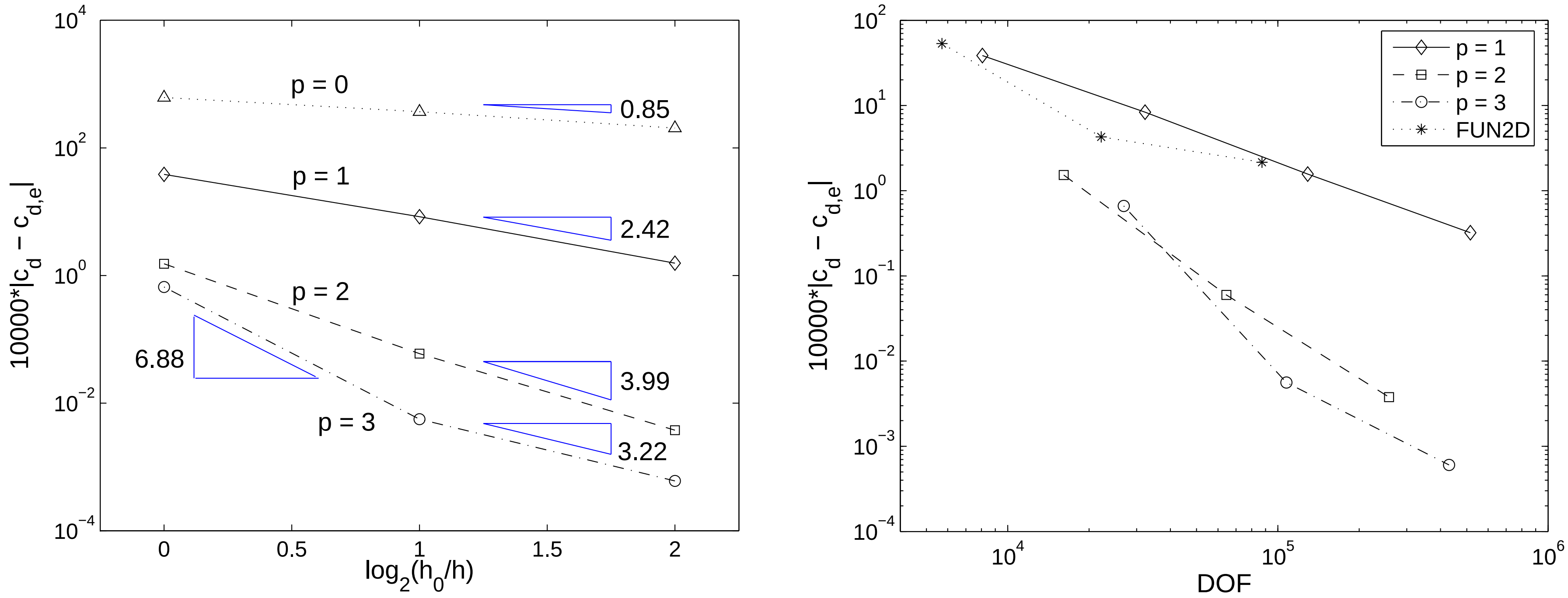


2112 element mesh

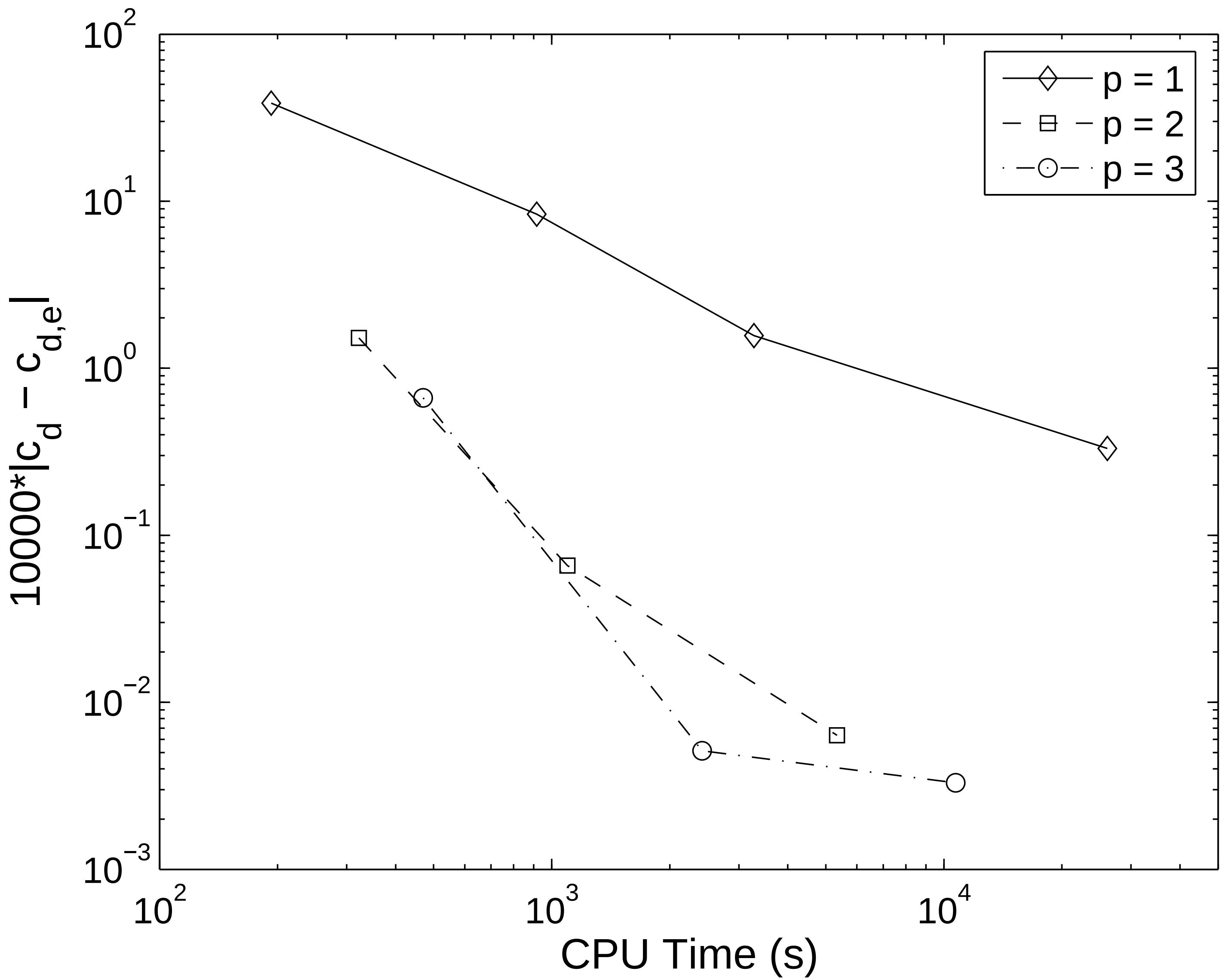


Mach contours

Drag Error Convergence



CPU Timing



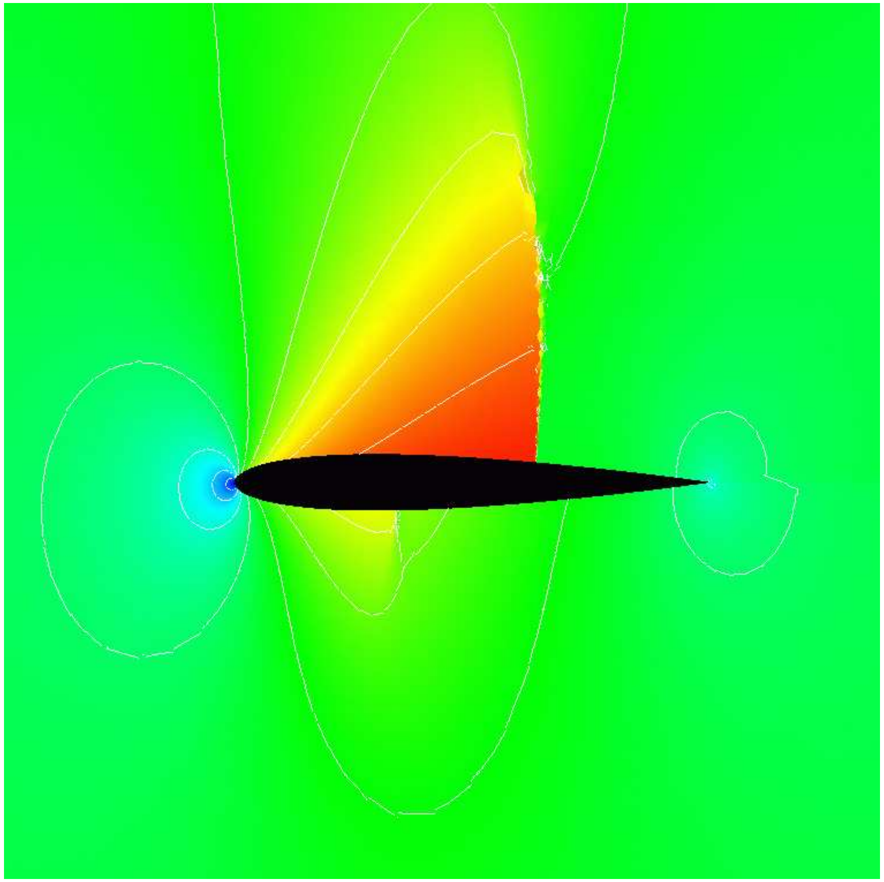
10^2
10^1
10^0
10^{-1}
10^{-2}
10^{-3}
10^2
10^3
10^4
CPU Time (s)
10000*|c_d − c_d,e|
p = 1
p = 2
p = 3

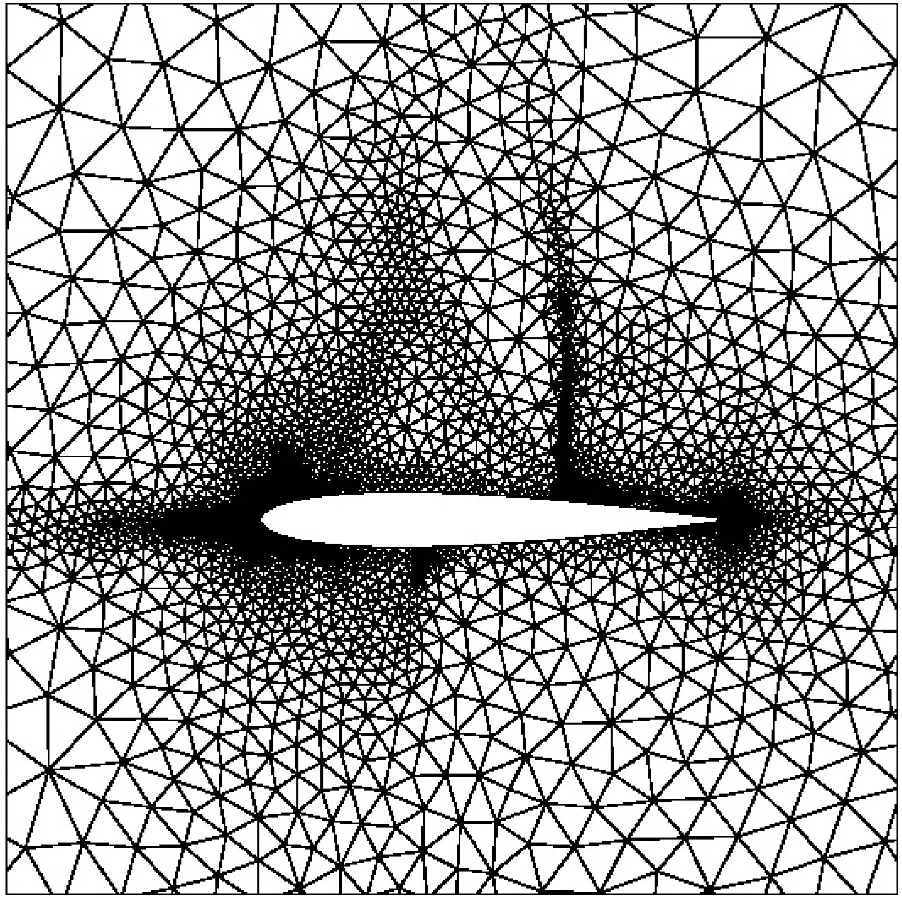
h-Adaptation

- For smooth flows, large high-order elements are ideal for accuracy and efficiency
- When singularities are present, h-adaptation is necessary to maintain accuracy
- Where to adapt? One option is output-based adaptation (Venditti & Darmofal)
  - Pick output of interest (lift, drag) and a desired error tolerance
  - Solve for output adjoint in addition to the flow solution
  - Use adjoint and flow solutions to estimate which elements contribute most/least to output error
  - Refine/coarsen mesh until the output error tolerance is met

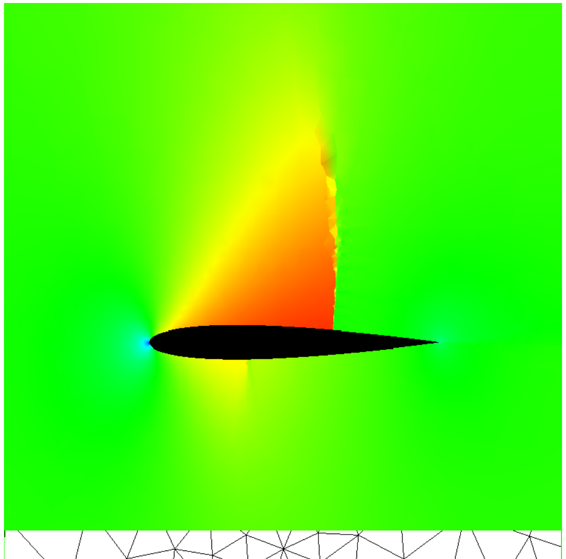
h-Adaptation Example

NACA 0012 Transonic test case: $M = 0.8$, $\alpha = 1.25^o$

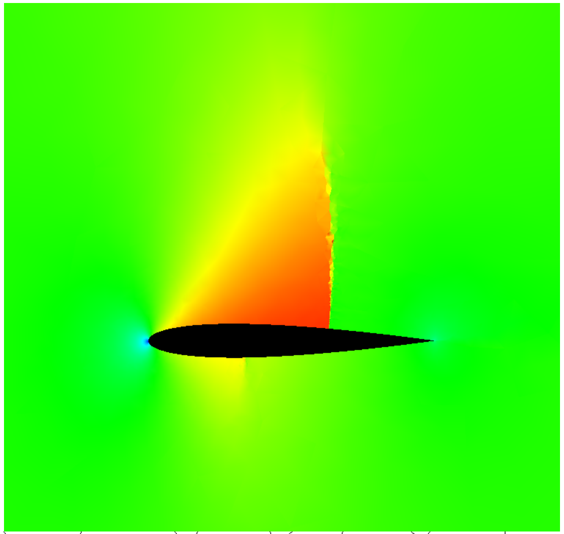


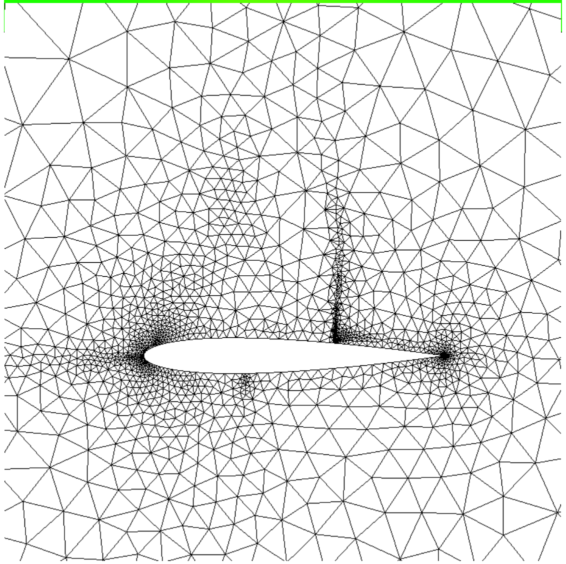


NACA 0012: $M = 0.8$, $\alpha = 1.25^o$

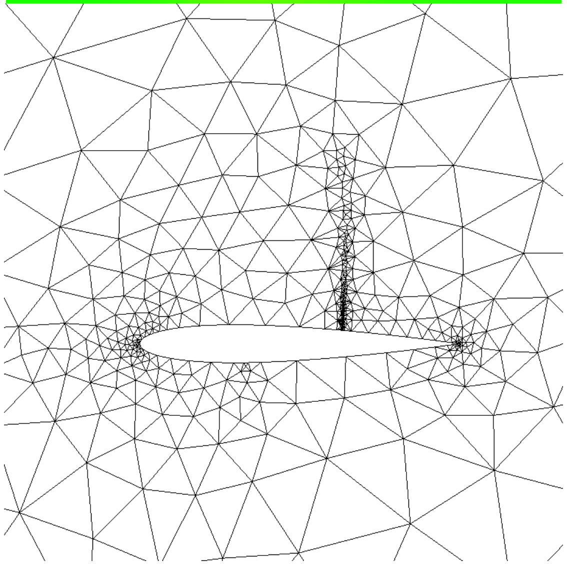


$\Leftarrow$ P1
49,836 DOF
$|C_d - C_{d,\text{exact}}| =$
$4.0 * 10^{-5}$





P2 $\Rightarrow$
30,288 DOF
$|C_d - C_{d,\text{exact}}| =$
$1.2 * 10^{-5}$



Ongoing Work

- Turbulence modeling (Todd Oliver)
- Shocks (Garrett Barter)
- Adaptation (Mike Park and Chris Fidkowski)
- Optimization (James Lu)
- Unsteady + Frequency Domain Solver (Tan Bui)
- Axisymmetric Solver + Plasma Physics (Shannon Cheng)
- Explicit solver (Pete Whitney)
- Hypersonic Flow (Doug Quattrochi)

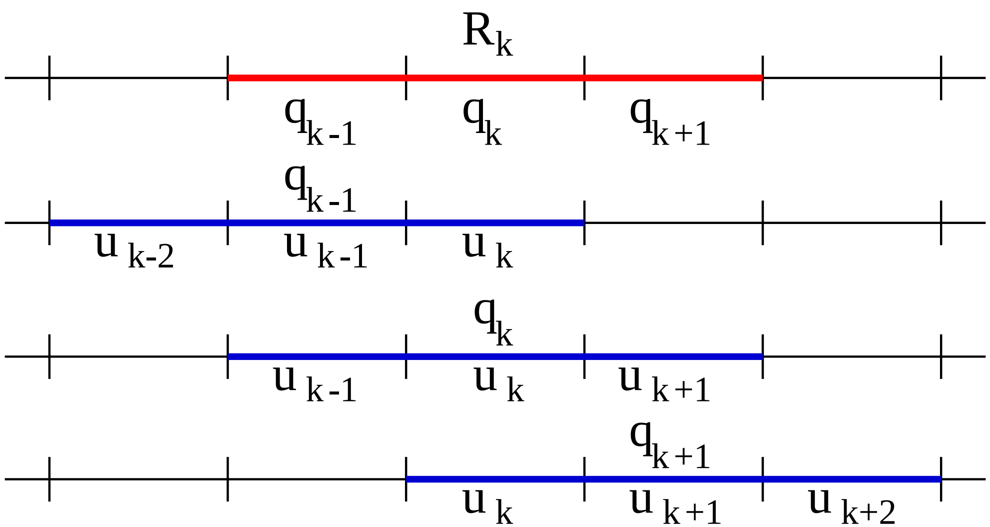
Questions?

BR1 Scheme

- No upwinding mechanism $\Rightarrow$ choose central fluxes

$$\widehat{u} = \frac{1}{2}(u_h^L + u_h^R); \quad \widehat{q} = \frac{1}{2}(q_h^L + q_h^R)$$

- Sub-optimal order of accuracy for odd p
- Stencil no longer compact



BR1 Scheme

- Define jump, $[\![\cdot]\!]$, and average, $\{\cdot\}$, operators:

$$[\![s]\!] = s^L - s^R \quad \text{and} \quad \{s\} = \frac{1}{2}(s^L + s^R)$$

- Central fluxes become

$$\widehat{u} = \{u_h\}; \quad \widehat{q} = \{(u_h)_x\} - \{\delta\}$$

- δ given by following problem: Find $\delta \in \mathcal{V}_h^p$ such that $\forall \tau_h \in \mathcal{V}_h^p$,

$$\sum_{\kappa \in T_h} \int_\kappa \tau_h \delta dx = \sum_n \left[[\![u_h]\!] \{\tau_h\} \right]$$

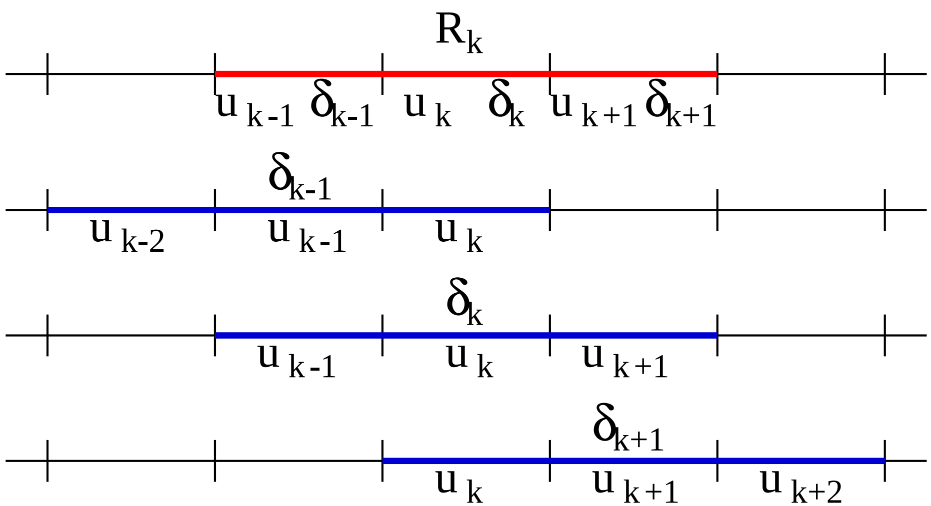
BR1 Scheme

- BR1 becomes: Find $u_h \in \mathcal{V}_h^p$ and such that $\forall v_h \in \mathcal{V}_h^p$,

$$\sum_{\kappa \in T_h} \int_\kappa (v_h)_x (u_h)_x dx$$

$$- \sum_n \left[[\![u_h]\!]\{(v_h)_x\} + [\![v_h]\!](\{(u_h)_x\} - \{\delta\}) \right] = \sum_{\kappa \in T_h} \int_\kappa v_h f dx$$

- Stencil extended by δ dependence on u_h



BR2 Scheme

- Goal: Eliminate extended stencil
- Approach: Modify auxiliary variable, δ, previously defined by:

$$\sum_{\kappa \in T_h} \int_{\kappa} \tau_h \delta dx = \sum_{n} \left[[\![u_h]\!] \{\tau_h\} \right]$$

- New variable, δ_f, given by: Find $\delta_f \in \mathcal{V}_h^p$ such that $\forall \tau_h \in \mathcal{V}_h^p$,

$$\int_{\kappa^{L/R}} \tau_h \delta_f^{L/R} dx = \left[[\![u_h]\!] \{\tau_h\}^{L/R} \right]_{n_f}$$

- New fluxes have same form as before

$$\widehat{u} = \{u_h\}; \quad \widehat{q} = \{(u_h)_x\} - \eta_f \{\delta_f\}$$

BR2 Scheme

- Replacing $\{\delta\}$ in BR1 by $\eta_f\{\delta_f\}$ gives BR2
- For proper choice of η_f, can prove optimal order of accuracy
- Stencil is compact