

Entropy-Based Mesh Refinement, I: The Entropy Adjoint Approach

2009 AIAA CFD Conference

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June 23, 2009

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Increasing interest in solution-based adaptive methods in CFD

- Complex problems often exhibit a wide range of length scales whose distribution is not known *a priori*
- Questions of robustness and solution accuracy persist even “routine” calculations

Variety of adaptive indicators available

- **Heuristic:** generally cheap but not robust
- **Rigorous:** robust but often expensive

We propose an **entropy adjoint** indicator that is somewhat of a compromise between heuristics and theory

Output error: difference between an output computed with the discrete system solution and that computed with the exact solution

$$\delta J = J_H(\mathbf{u}_H) - J(\mathbf{u})$$

$\mathbf{u}_H \in \mathcal{V}_H =$ approximate solution, $\mathbf{u} \in \mathcal{V} =$ exact solution

Adjoint-based output error estimation techniques

- Account for propagation effects inherent to hyperbolic problems
- Identify all areas of the domain that are important for the accurate prediction of an output
- Require solution of an adjoint equation

The Continuous Adjoint

Primal equation

$$\mathbf{r}(\mathbf{u}) = 0, \text{ on } \Omega$$

The continuous adjoint, ψ , is a Lagrange multiplier for

$$\mathcal{L} = J(\mathbf{u}) - \int_{\Omega} \psi^T \mathbf{r}(\mathbf{u}) d\Omega$$

Requiring a stationary Lagrangian for permissible state variations, $\delta \mathbf{u} \in \mathcal{V}^{\text{perm}}$, yields (in weak form) the

Adjoint equation

$$J'[\mathbf{u}](\delta \mathbf{u}) - \int_{\Omega} \psi^T \mathbf{r}'[\mathbf{u}](\delta \mathbf{u}) d\Omega = 0, \quad \forall \delta \mathbf{u} \in \mathcal{V}^{\text{perm}}$$

Example: First-Order Conservation Laws

Consider a system of conservation laws in quasi-linear form,

$$\mathbf{r}(\mathbf{u}) = \mathbf{A}_i \partial_i \mathbf{u} = 0$$

The adjoint equation is, after an integration by parts,

$$J'[\mathbf{u}](\delta \mathbf{u}) + \int_{\Omega} \partial_i \psi^T \mathbf{A}_i \delta \mathbf{u} d\Omega - \int_{\partial\Omega} \psi^T \mathbf{A}_i \delta \mathbf{u} n_i ds = 0, \quad \forall \delta \mathbf{u} \in \mathcal{V}^{\text{perm}}$$

If $J(\mathbf{u})$ is an integral on $\partial\Omega$, ψ must satisfy

$$\mathbf{A}_i^T \partial_i \psi = 0, \quad \text{in } \Omega,$$

subject to the boundary conditions

$$J'[\mathbf{u}](\delta \mathbf{u}) - \int_{\partial\Omega} \psi^T \mathbf{A}_i \delta \mathbf{u} n_i ds = 0, \quad \forall \delta \mathbf{u} \in \mathcal{V}^{\text{perm}}$$

Output Error Estimation with Adjoint

- 1 $\mathbf{u}_H \in \mathcal{V}_H$ will generally not satisfy the analytical PDE: $\mathbf{r}(\mathbf{u}_H) \neq 0$
- 2 If $\delta\mathbf{u} \equiv \mathbf{u}_H - \mathbf{u}$ is small, we can write

$$\mathbf{r}(\mathbf{u}_H) = \mathbf{r}(\mathbf{u} + \delta\mathbf{u}) \approx \mathbf{r}'[\mathbf{u}](\delta\mathbf{u})$$

- 3 Using the adjoint equation we have

$$\delta J \approx J'[\mathbf{u}](\delta\mathbf{u}) = \int_{\Omega} \psi^T \mathbf{r}'[\mathbf{u}](\delta\mathbf{u}) \approx \int_{\Omega} \psi^T \mathbf{r}(\mathbf{u}_H)$$

The output error is given by an adjoint-weighted residual

- Above is only an estimate when the output or equations are nonlinear and the perturbations are finite
- The estimate can be localized to yield an adaptive indicator

Entropy Adjoint Connection

Two disadvantages of adjoint-based output error estimation

- 1 Adjoint solution is required for each output
- 2 Only requested outputs are targeted

We seek a *general purpose* adaptive indicator that

- does not require solution of an adjoint problem
- produces an “overall good” solution

One promising approach makes use of the **entropy variables**

Starting point (first-order conservation laws):

$$\underbrace{\mathbf{r}(\mathbf{u}) = \mathbf{A}_i \partial_i \mathbf{u} = 0}_{\text{primal equation}}, \quad \underbrace{\partial_i F_i = 0}_{\text{entropy conservation}}$$

$F_i(\mathbf{u})$ is the entropy flux associated with an entropy function $U(\mathbf{u})$

Entropy Adjoint Connection (ctd.)

- The entropy pair $(U(\mathbf{u}), F_i(\mathbf{u}))$ must satisfy $U_{\mathbf{u}}\mathbf{A}_i = (F_i)_{\mathbf{u}}$
- The **entropy variables** are defined by

$$\mathbf{v} \equiv U_{\mathbf{u}}^T$$

The entropy variables symmetrize the equations in the sense that

- 1 \mathbf{u}_v is symmetric, positive definite
- 2 $\mathbf{A}_i\mathbf{u}_v$ is symmetric

Using these symmetry properties, we have

$$0 = \mathbf{A}_i\partial_i\mathbf{u} = \mathbf{A}_i\mathbf{u}_v\partial_i\mathbf{v} = \mathbf{u}_v\mathbf{A}_i^T\partial_i\mathbf{v} \Rightarrow \mathbf{A}_i^T\partial_i\mathbf{v} = 0$$

The entropy variables satisfy the adjoint equation! (BCs too)

Entropy Adjoint Connection (ctd.)

We examine the adjoint-weighted residual to deduce the output:

$$\begin{aligned}\delta J &= \int_{\Omega} \mathbf{v}^T \delta \mathbf{r} \, d\Omega = \int_{\Omega} \mathbf{v}^T \mathbf{A}_i \partial_i \delta \mathbf{u} \, d\Omega \\ &= - \int_{\Omega} \underbrace{\partial_i \mathbf{v}^T \mathbf{A}_i}_{=0} \delta \mathbf{u} \, d\Omega + \int_{\partial\Omega} \underbrace{\mathbf{v}^T \mathbf{A}_i}_{(F_i)_u} \delta \mathbf{u} \, n_i \, ds \\ &= \int_{\partial\Omega} (F_i)_u \delta \mathbf{u} \, n_i \, ds = \delta \left[\underbrace{\int_{\partial\Omega} F_i n_i \, ds}_J \right]\end{aligned}$$

J measures the net entropy flow out of the domain

Second-Order Conservation Laws

Primal equation:

$$\mathbf{r}(\mathbf{u}) = \mathbf{A}_i \partial_i \mathbf{u} - \partial_i (\mathbf{K}_{ij} \partial_j \mathbf{u}) = 0$$

- Viscous dissipation is a source term in the adjoint equation for \mathbf{v}

The entropy variables serve as an “adjoint” solution for

$$J = \underbrace{\int_{\partial\Omega} F_i n_i ds}_{\text{outflow of } U} + \underbrace{\int_{\Omega} \partial_i \mathbf{v}^T \tilde{\mathbf{K}}_{ij} \partial_j \mathbf{v} d\Omega}_{\text{generation of } U} - \underbrace{\int_{\partial\Omega} \mathbf{v}^T \tilde{\mathbf{K}}_{ij} \partial_j \mathbf{v} n_i ds}_{\text{diffusion of } U}$$

where $\tilde{\mathbf{K}}_{ij} \equiv \mathbf{K}_{ij} \mathbf{u}_v$ is symmetrized in the sense that $\tilde{\mathbf{K}}_{ij} = \tilde{\mathbf{K}}_{ji}^T$

- The expression for J is an entropy balance statement: $J(\mathbf{u}) = 0$
- The terms in J do not necessarily balance for \mathbf{u}_H

Using the Entropy Variables

The entropy variables are readily computable from \mathbf{u} ,

$$\mathbf{v} = U_{\mathbf{u}}^T = \left[\frac{\gamma - S}{\gamma - 1} - \frac{1}{2} \frac{\rho V^2}{\rho}, \frac{\rho u_i}{\rho}, -\frac{\rho}{\rho} \right]^T,$$

where the entropy function U is

$$U = -\rho S / (\gamma - 1), \quad S = \ln p - \gamma \ln \rho,$$

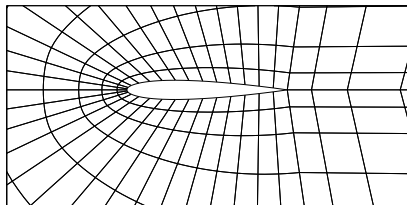
Approach

Use \mathbf{v} as an adjoint solution in output error estimation

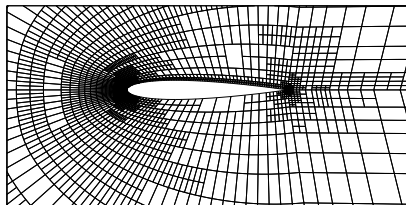
- Targeted areas are those where **entropy generation** or **entropy transport** is not predicted well
- Similar to adapting on residual of entropy transport equation
- *Separate adjoint solve is not required*

Implementation

- Discontinuous Galerkin (DG) finite element discretization
- Discrete adjoint solution
- Error estimation performed on order $p + 1$ space (same mesh)
- Fixed-fraction, isotropic, hanging-node adaptation
- Curved, body-fitted quadrilateral and hexahedral meshes



Sample initial mesh

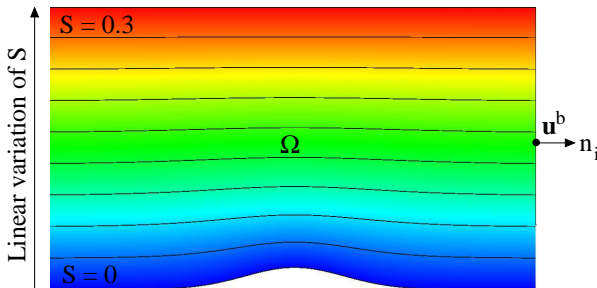


Sample adapted mesh

Verification of the Entropy Adjoint Connection

Compare the entropy variables, \mathbf{v}_h , to the discrete adjoint, ψ_h , for

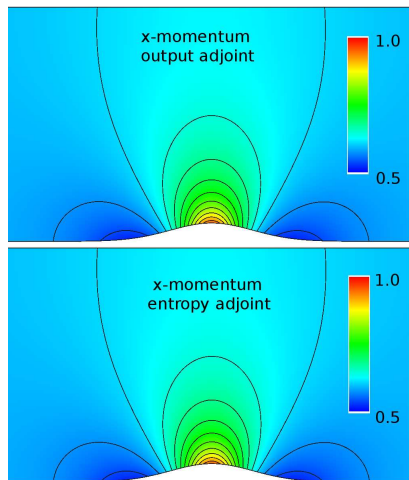
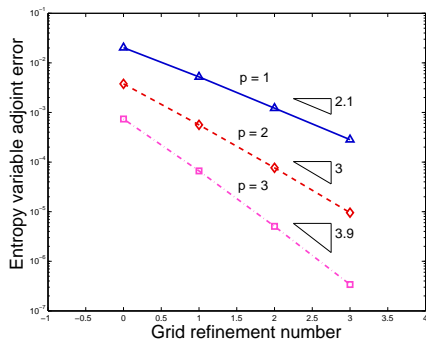
$$J_h = \int_{\partial\Omega} F_i(\mathbf{u}_h^b) n_i ds$$



Compute: (Entropy variable adjoint error) $^2 = \int_{\Omega} \|\psi_h - \mathbf{v}_h\|_2^2 d\Omega$

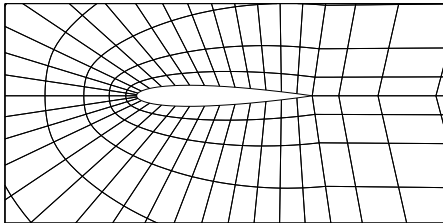
Verification of the Entropy Adjoint Connection (ctd.)

Behavior of entropy variable adjoint error under uniform refinement



- Error decreases at $O(h^{p+1})$
- The entropy variables are indeed adjoint solutions

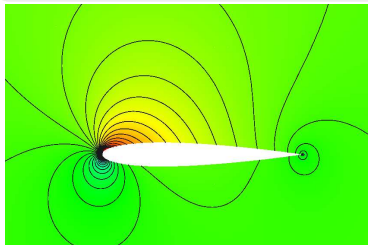
- Hanging-node adaptation
- fixed fraction: 10%
- $q = 5$ geometry representation
- Quadrilateral meshes
- $p = 2$ solution interpolation
- Measured lift and drag



Initial mesh

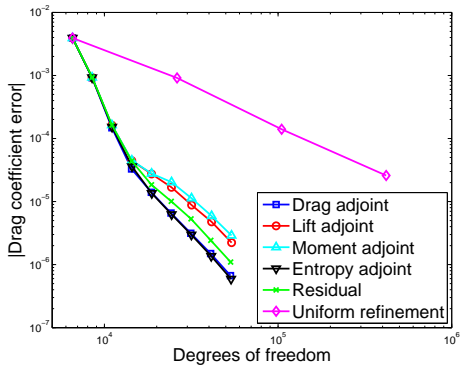
Indicators

- 1 Drag adjoint
- 2 Lift adjoint
- 3 Moment adjoint
- 4 Entropy adjoint
- 5 Residual

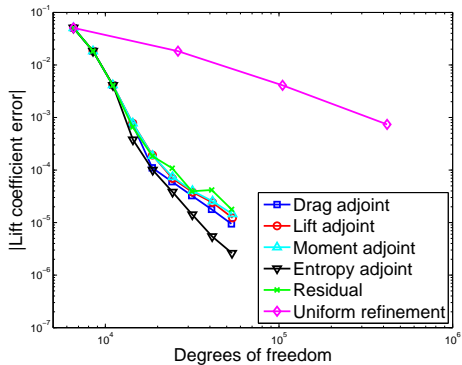


Mach contours

- Degree of freedom (DOF) versus output error for $p = 2$
- Entropy adjoint performance is comparable to output adjoints

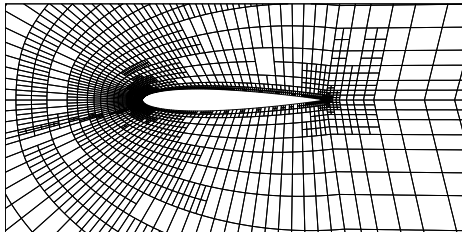


Drag Error

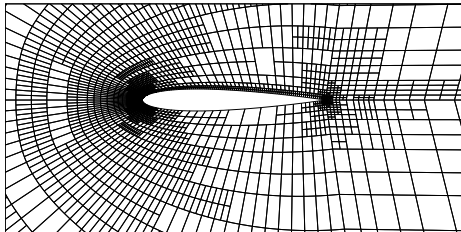


Lift Error

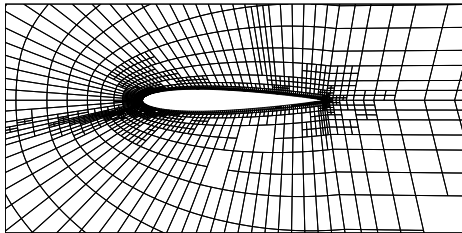
NACA 0012, $M = 0.4$, $\alpha = 5^\circ$, Final Meshes



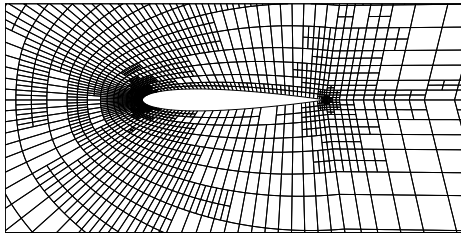
Drag Adjoint



Entropy Adjoint

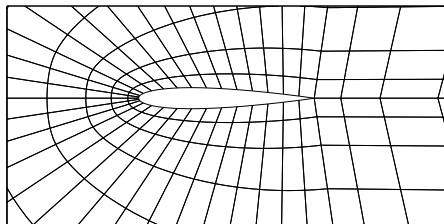


Lift Adjoint



Residual

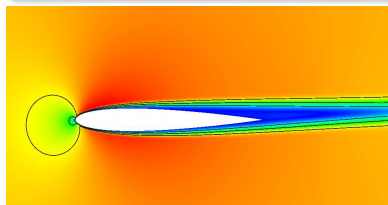
- Hanging-node adaptation
- fixed fraction: 10%
- $q = 3$ geometry representation
- Quadrilateral meshes
- $p = 2$ solution interpolation
- Measured lift and drag



Initial mesh

Indicators

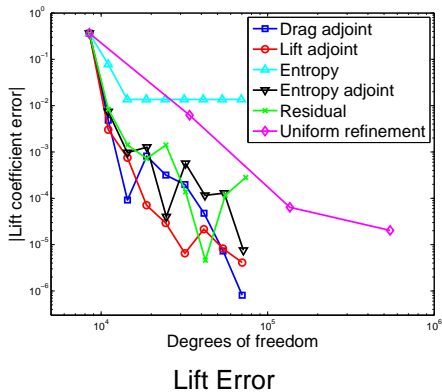
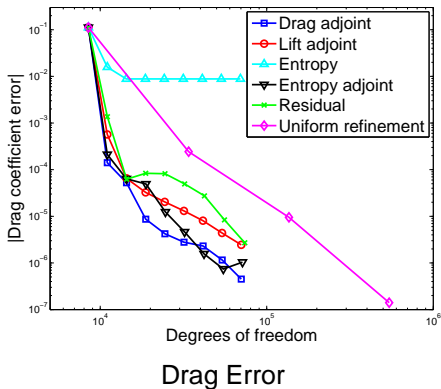
- 1 Drag adjoint
- 2 Lift adjoint
- 3 Entropy adjoint
- 4 Residual
- 5 Entropy



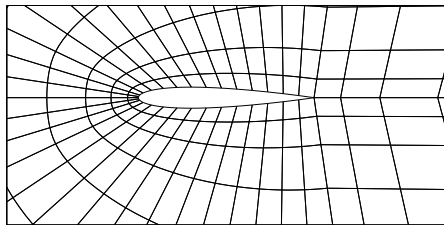
Mach contours

NACA 0012, $M = 0.5$, $\alpha = 2^\circ$, $Re = 5k$

- Degree of freedom (DOF) versus output error for $p = 2$
- Entropy adjoint performance is comparable to output adjoints



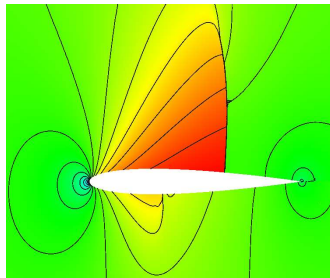
- Hanging-node adaptation
- fixed fraction: 10%
- $q = 3$ geometry representation
- Element-constant artificial viscosity
- $p = 2$ solution interpolation
- Measured lift and drag



Initial mesh

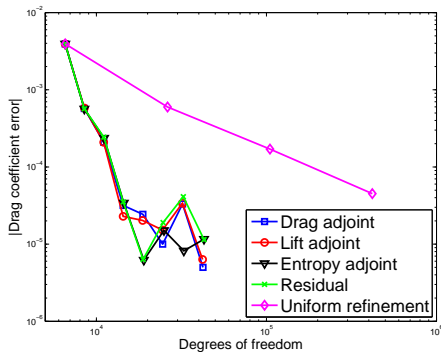
Indicators

- 1 Drag adjoint
- 2 Lift adjoint
- 3 Entropy adjoint
- 4 Residual

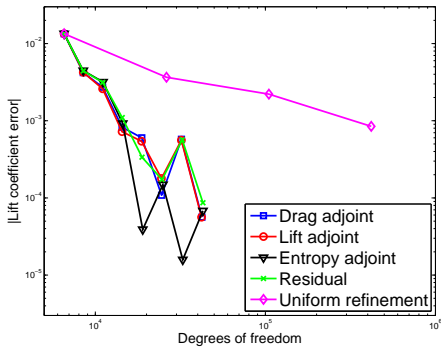


Mach contours

- Degree of freedom (DOF) versus output error for $p = 2$
- More noise in results – entropy adjoint still performs well

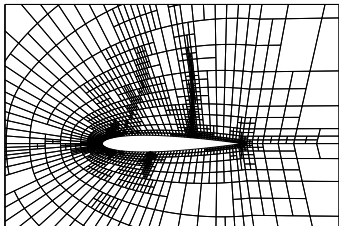


Drag

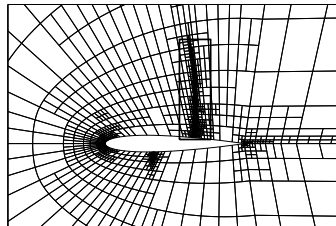


Lift

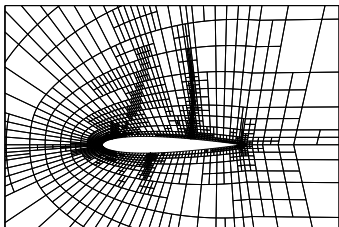
NACA 0012, $M = 0.8$, $\alpha = 1.25^\circ$, Final Meshes



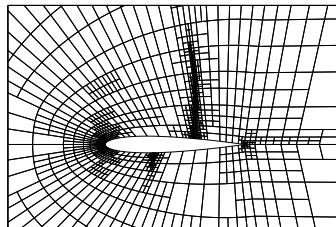
Drag Adjoint (2990)



Entropy Adjoint (2814)



Lift Adjoint (2997)



Residual (2372)

Conclusions

- Output error estimation based on adjoint solutions is a rigorous, but somewhat expensive, approach for targeting select output quantities of interest
- The entropy variables satisfy an adjoint equation; the resulting “entropy adjoint” indicator is cheap to compute and targets errors in entropy generation and transport
- Performance of the entropy adjoint indicator is comparable to standard output adjoints for the flows tested

Ongoing work

- Extension to unsteady flows (entropy adjoint connection holds)
- Application to other conservation laws with an entropy extension
- Relationship to engineering output quantities

Acknowledgements

- **P.L. Roe** acknowledges hospitality at the Department of Applied Mathematics and Theoretical Physics, University of Cambridge UK, and the financial support of a William Penney Fellowship from the UK Ministry of Defence
- **K.J. Fidkowski** acknowledges the support of the University of Michigan, Ann Arbor